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3. EVALUATION OF RESULTS AND RECOMMENDATIONS

This section presents and discusses the results generated in the CFD simulations for 101 different room configurations. The detailed flow patterns for each room are not discussed; the comparisons focus on the quantitative analysis of the CFD data.

The analysis concentrates on eight parameters defined in section 2.4.2:

- Mean cage temperatures
- Mean cage CO₂ concentrations
- Mean cage relative humidity (RH)
- Mean cage NH₃ concentration on day 4
- Mean room breathing zone temperature
- Mean room breathing zone CO₂ concentration
- Mean room breathing zone (RH)
- Mean room breathing zone NH₃ concentration on day 4

As each day had a different NH₃ generation rate, the NH₃ concentrations are different on each day. However as the underlying mass fraction information and RH information does not change on a daily basis in the simulations, room performance can be compared by using the results for any of the 10 days. For ease of comparison, results are presented for day 4, which corresponds to the day most widely used to change the bedding in the mice cages.

In addition to the day 4 NH₃ concentrations (i.e., the conditions that would arise four days after clean bedding is placed in every cage), a summary of the complete 10-day cycle is presented.

The analysis focuses on trends in the data that identify any ventilation schemes as particularly good or bad, and recommendations are made. The major recommendation is tested by further post-processing of the CFD data.

3.1 Results for 101 Room Simulations

Figures 3.01 to 3.08 show bar charts of the eight parameters identified as important in categorizing the behavior of the ventilation system on the room and the cages. The individual cases can be identified by comparison of the case number on the bottom of the charts with the complete list of cases in table 3.01 below.

Table 3.01 List of All Whole Room Runs

Case Name	Supply Diffuser Type	Exhaust Location and Number	Change Station (Design/ Status)	Rack Orientation	Rack Density	Pressure of Room to Corridor	Supply Temperature °C (°F)	Supply ACH
Basecase	Radial	Ceiling (x2)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 02	Radial	High (x4)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 03	Radial	Low (x4)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 04	Slot	Ceiling (x2)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 05	Slot	High (x4)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 06	Slot	Low (x4)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 07	Low Ind	Ceiling (x2)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 08	Low Ind	High (x4)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 09	Low Ind	Low (x4)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 10	Radial	Ceiling (x2)	Thoren/ OFF	Parallel	Single	Neg.. 100cfm	20.7 (69.3)	15
Case 11	Radial	Low (x4)	Thoren/ OFF	Parallel	Single	Neg.. 100cfm	20.7 (69.3)	15
Case 12	Slot	Ceiling (x2)	Thoren/ OFF	Parallel	Single	Neg.. 100cfm	20.7 (69.3)	15
Case 13	Slot	Low (x4)	Thoren/ OFF	Parallel	Single	Neg.. 100cfm	20.7 (69.3)	15
Case 14	Low Ind	Ceiling (x2)	Thoren/ OFF	Parallel	Single	Neg.. 100cfm	20.7 (69.3)	15
Case 15	Low Ind	Low (x4)	Thoren/ OFF	Parallel	Single	Neg.. 100cfm	20.7 (69.3)	15
Case 16	Radial	Ceiling (x2)	Thoren/ ON	Parallel	Single	Pos.. 100cfm	18.8 (65.8)	15
Case 17	Slot	Ceiling (x2)	Thoren/ ON	Parallel	Single	Pos.. 100cfm	18.8 (65.8)	15
Case 18	Low Ind	Ceiling (x2)	Thoren/ ON	Parallel	Single	Pos.. 100cfm	18.8 (65.8)	15
Case 19	Radial	Ceiling (x2)	Thoren/ ON	Perpendicular	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 20	Slot	Ceiling (x2)	Thoren/ ON	Perpendicular	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 21	Low Ind	Ceiling (x2)	Thoren/ ON	Perpendicular	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 22	Radial	Low (x4)	Thoren/ ON	Perpendicular	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 23	Slot	Low (x4)	Thoren/ ON	Perpendicular	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 24	Low Ind	Low (x4)	Thoren/ ON	Perpendicular	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 25 *	Radial	Ceiling (x2)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 26 *	Slot	Ceiling (x2)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 27 *	Low Ind	Ceiling (x2)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 28	Low Ind	Low (x4)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	16.8 (62.2)	10
Case 29	Low Ind	Low (x4)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	11.0 (51.8)	5
Case 30	Low Ind	Low (x4)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	19.8 (67.6)	20
Case 31	Radial	Low (x4)	Thoren/ ON	Perpendicular	Double	Neg.. 100cfm	17.5 (63.5)	15
Case 32	Slot	Low (x4)	Thoren/ ON	Perpendicular	Double	Neg.. 100cfm	17.5 (63.5)	15
Case 33	Low Ind	Low (x4)	Thoren/ ON	Perpendicular	Double	Neg.. 100cfm	17.5 (63.5)	15
Case 34	Radial	Ceiling (x2)	Thoren/ ON	Perpendicular	Double	Neg.. 100cfm	17.5 (63.5)	15
Case 35	Slot	Ceiling (x2)	Thoren/ ON	Perpendicular	Double	Neg.. 100cfm	17.5 (63.5)	15
Case 36	Low Ind	Ceiling (x2)	Thoren/ ON	Perpendicular	Double	Neg.. 100cfm	17.5 (63.5)	15
Case 37	Radial	Ceiling (x1) / Low (x4) (Mass flow in 50/50 split)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 38	Slot	Ceiling (x1) / Low (x4) (Mass flow in 50/50 split)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 39	Low Ind	Ceiling (x1) / Low (x4) (Mass flow in 50/50 split)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15
Case 40	Radial	Ceiling (x4)	Thoren/ ON	Parallel	Single	Neg.. 100cfm	18.8 (65.8)	15

Case Name	Supply Diffuser Type	Exhaust Location and Number	Change Station (Design/ Status)	Rack Orientation	Rack Density	Pressure of Room to Corridor	Supply Temperature °C (°F)	Supply ACH
Case 69	Radial	High (x4) / Low (x4) (Mass flow split evenly amongst exhausts)	Thoren/ ON	Parallel	Single	Neg. 100cfm	18.8 (65.8)	15
Case 70	Slot	High (x4) / Low (x4) (Mass flow split evenly amongst exhausts)	Thoren/ ON	Parallel	Single	Neg. 100cfm	18.8 (65.8)	15
Case 71	Low Ind	High (x4) / Low (x4) (Mass flow split evenly amongst exhausts)	Thoren/ ON	Parallel	Single	Neg. 100cfm	18.8 (65.8)	15
Case 72	Radial	High (x4) / Low (x2) (Mass flow split evenly amongst exhausts)	Thoren/ ON	Parallel	Single	Neg. 100cfm	18.8 (65.8)	15
Case 73	Slot	High (x4) / Low (x2) (Mass flow split evenly amongst exhausts)	Thoren/ ON	Parallel	Single	Neg. 100cfm	18.8 (65.8)	15
Case 74	Low Ind	High (x4) / Low (x2) (Mass flow split evenly amongst exhausts)	Thoren/ ON	Parallel	Single	Neg. 100cfm	18.8 (65.8)	15
Case 75	Radial	Ceiling (x1) / Low (x4) (Mass flow in 50/50 split)	Lab. Prod. / ON	Parallel	Single	Neg. 100cfm	18.8 (65.8)	15
Case 76 **	Radial	Ceiling (x2)	Thoren/ ON	Parallel	Single	Neg. 100cfm	19.2 (66.6)	15
Case 77 **	Slot	Ceiling (x2)	Thoren/ ON	Parallel	Single	Neg. 100cfm	19.2 (66.6)	15
Case 78 **	Low Ind	Ceiling (x2)	Thoren/ ON	Parallel	Single	Neg. 100cfm	19.2 (66.6)	15
Case 79	Radial	2 Door exhausts	Thoren/ ON	Parallel	Single	Neg. 100cfm	18.8 (65.8)	15
Case 80	Slot	2 Door exhausts	Thoren/ ON	Parallel	Single	Neg. 100cfm	18.8 (65.8)	15
Case 81	Low Ind	2 Door exhausts	Thoren/ ON	Parallel	Single	Neg. 100cfm	18.8 (65.8)	15
Case 82	Radial	2 Door exhausts	Thoren/ ON	Parallel	Single	Neg. 100cfm	18.8 (65.8)	15
Case 83	Slot	2 Door exhausts	Thoren/ ON	Perpendicular	Double	Neg. 100cfm	17.5 (63.5)	15
Case 84	Low Ind	2 Door exhausts	Thoren/ ON	Perpendicular	Double	Neg. 100cfm	17.5 (63.5)	15
Case 85	Radial	Low (x4)	Lab. Prod. / ON	Perpendicular	Double	Neg. 100cfm	17.5 (63.5)	15
Case 86	Slot	Low (x4)	Lab. Prod. / ON	Perpendicular	Double	Neg. 100cfm	17.5 (63.5)	15
Case 87	Radial	Low (x4)	Thoren/ ON	Parallel	Reduced	Neg. 100cfm	19.2 (66.6)	15

Case Name	Supply Diffuser Type	Exhaust Location and Number	Change Station (Design/ Status)	Rack Orientation	Rack Density	Pressure of Room to Corridor	Supply Temperature °C (°F)	Supply ACH
Case 88	Slot	Low (x4)	Thoren/ ON	Parallel	Reduced	Neg. 100cfm	19.2 (66.6)	15
Case 89	Low Ind	Low (x4)	Thoren/ ON	Parallel	Reduced	Neg. 100cfm	19.2 (66.6)	15
Case 90	Radial	Ceiling (x2)	Thoren/ ON	Perpendicular all 5 on 1 wall	Single	Neg. 100cfm	18.8 (65.8)	15
Case 91	Slot	Ceiling (x2)	Thoren/ ON	Perpendicular all 5 on 1 wall	Single	Neg. 100cfm	18.8 (65.8)	15
Case 92	Low Ind	Ceiling (x2)	Thoren/ ON	Perpendicular all 5 on 1 wall	Single	Neg. 100cfm	18.8 (65.8)	15
Case 93	Radial	Ceiling (x2)	Thoren/ ON	Perpendicular all 5 on 1 wall	Double	Neg. 100cfm	17.5 (63.5)	15
Case 94	Slot	Ceiling (x2)	Thoren/ ON	Perpendicular all 5 on 1 wall	Double	Neg. 100cfm	17.5 (63.5)	15
Case 95	Low Ind	Ceiling (x2)	Thoren/ ON	Perpendicular all 5 on 1 wall	Double	Neg. 100cfm	17.5 (63.5)	15
Case 96	Radial	Ceiling (x2)	Lab. Prod. / ON	Perpendicular all 5 on 1 wall	Double	Neg. 100cfm	17.5 (63.5)	15
Case 97	Slot	Ceiling (x2)	Lab. Prod. / ON	Perpendicular all 5 on 1 wall	Double	Neg. 100cfm	17.5 (63.5)	15
Case 98	Low Ind	Ceiling (x2)	Lab. Prod. / ON	Perpendicular all 5 on 1 wall	Double	Neg. 100cfm	17.5 (63.5)	15
Case 99 ***	Radial	Ceiling (x2)	Thoren/ ON	Parallel	Single	Neg. 100cfm	22.2 (72.0)	15
Case 100 ***	Radial	Low (x4)	Thoren/ ON	Parallel	Single	Neg. 100cfm	22.2 (72.0)	15
Case 101 ***	Low Ind	Low (x4)	Lab. Prod. / ON	Perpendicular	Double	Neg. 100cfm	22.2 (72.0)	5

* Sealed cages instead of open cages

** Room 4.26m (14') wide instead of 3.66m (12')

*** Supply air temperature fixed at 22.2 °C (72.0 °F). In all other cases, the exhaust temperature was set to be 22.2 °C (72.0 °F) by setting the supply air temperature appropriately.

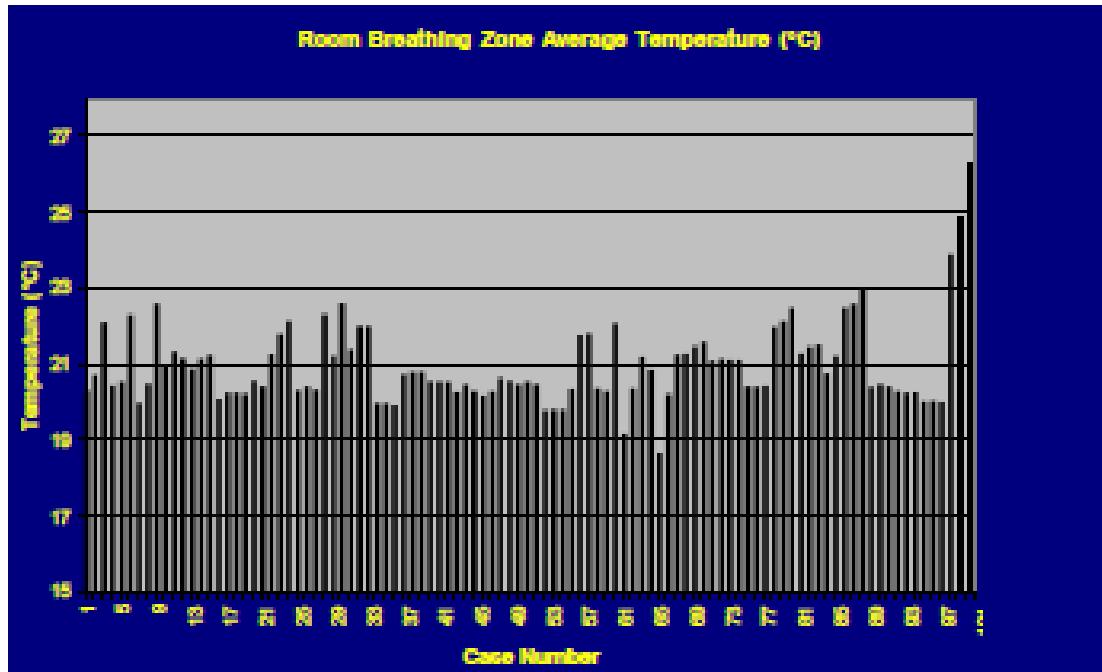


Figure 3.01 Mean Room Breathing Zone Temperature

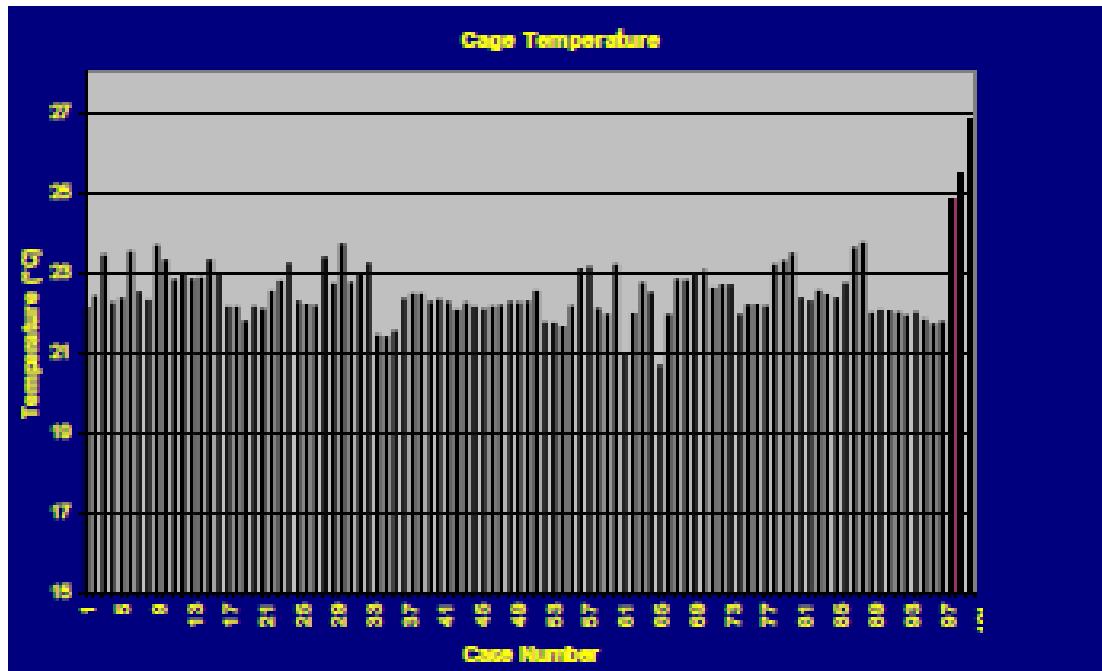


Figure 3.02 Mean Cage Temperatures

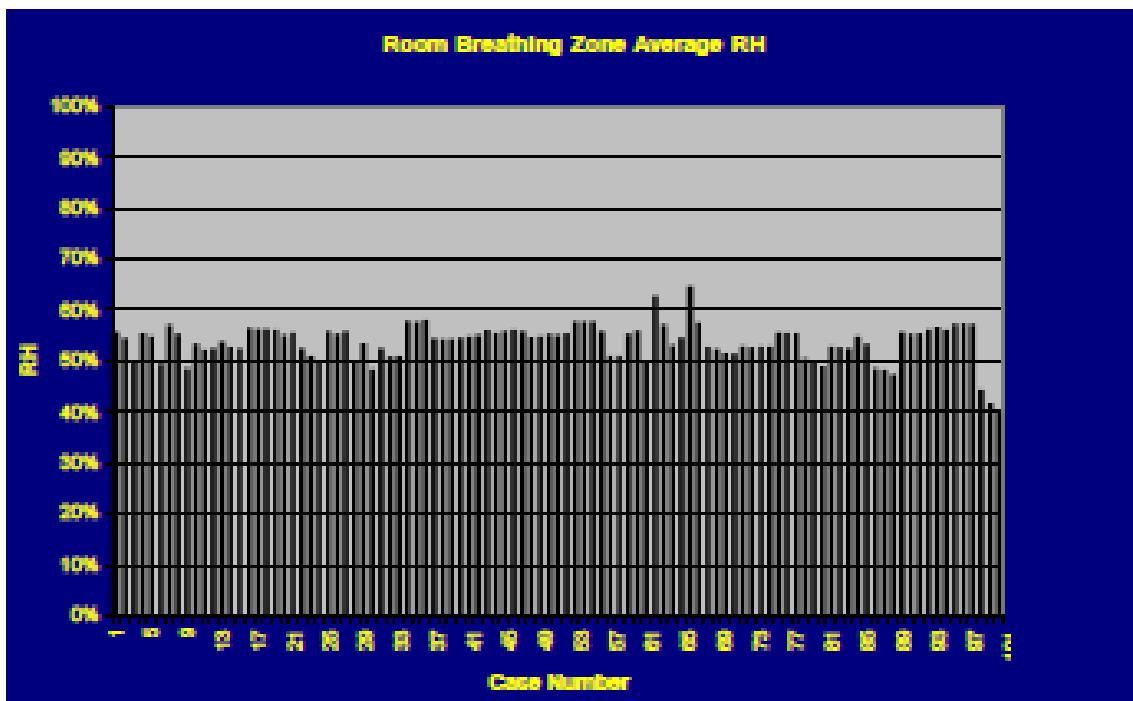


Figure 3.03 Mean Room Breathing Zone Relative Humidity (RH)

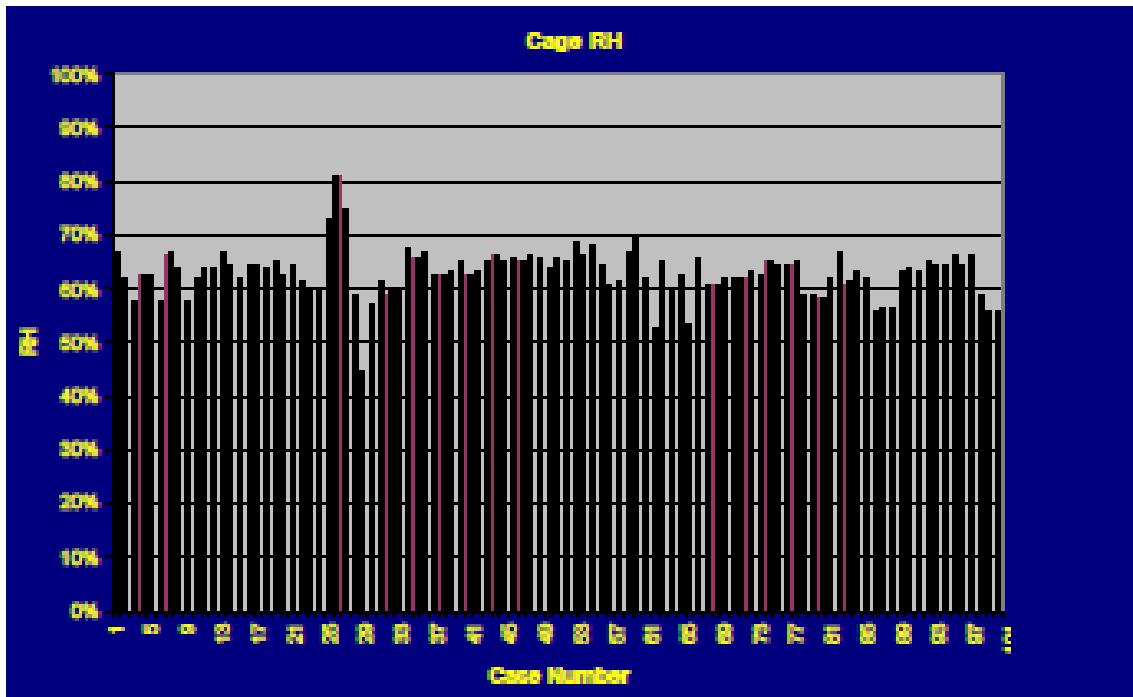


Figure 3.04 Mean Cage Relative Humidity (RH)

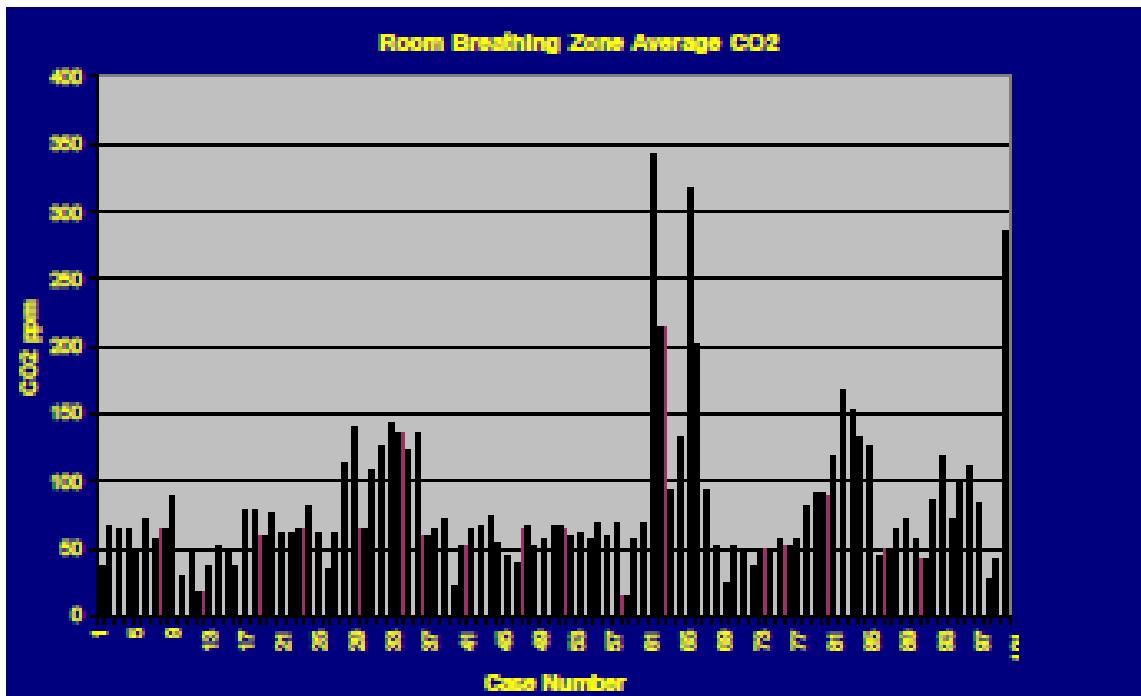


Figure 3.05 Mean Room Breathing Zone CO₂ Concentration

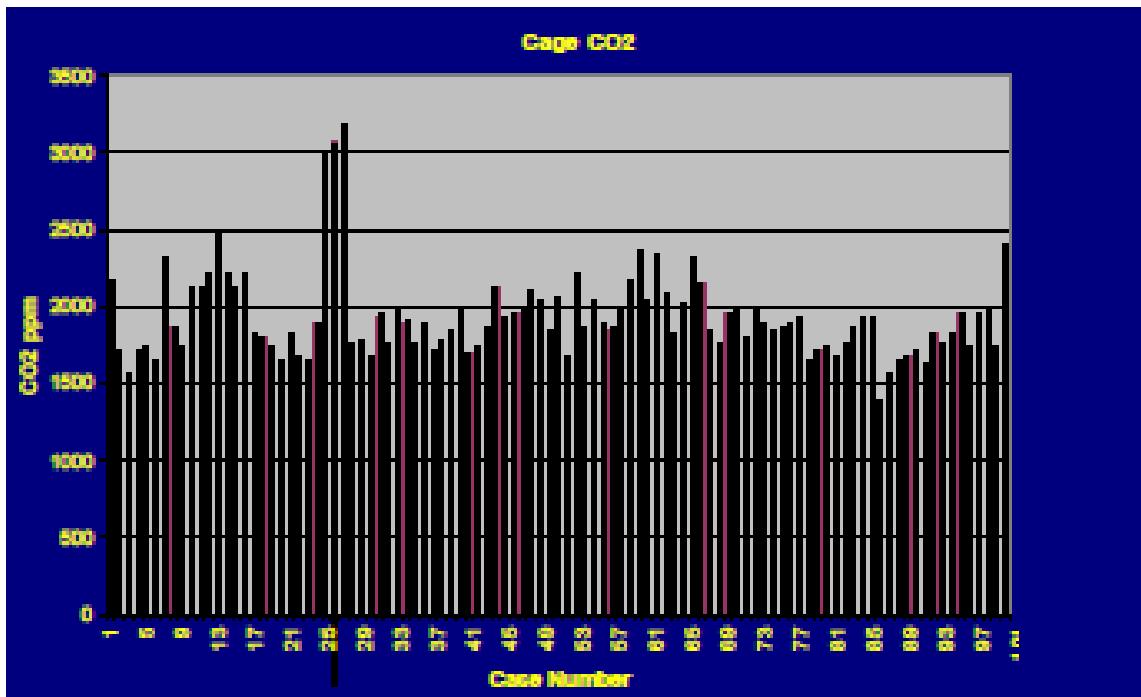


Figure 3.06 Mean Cage CO₂ Concentration

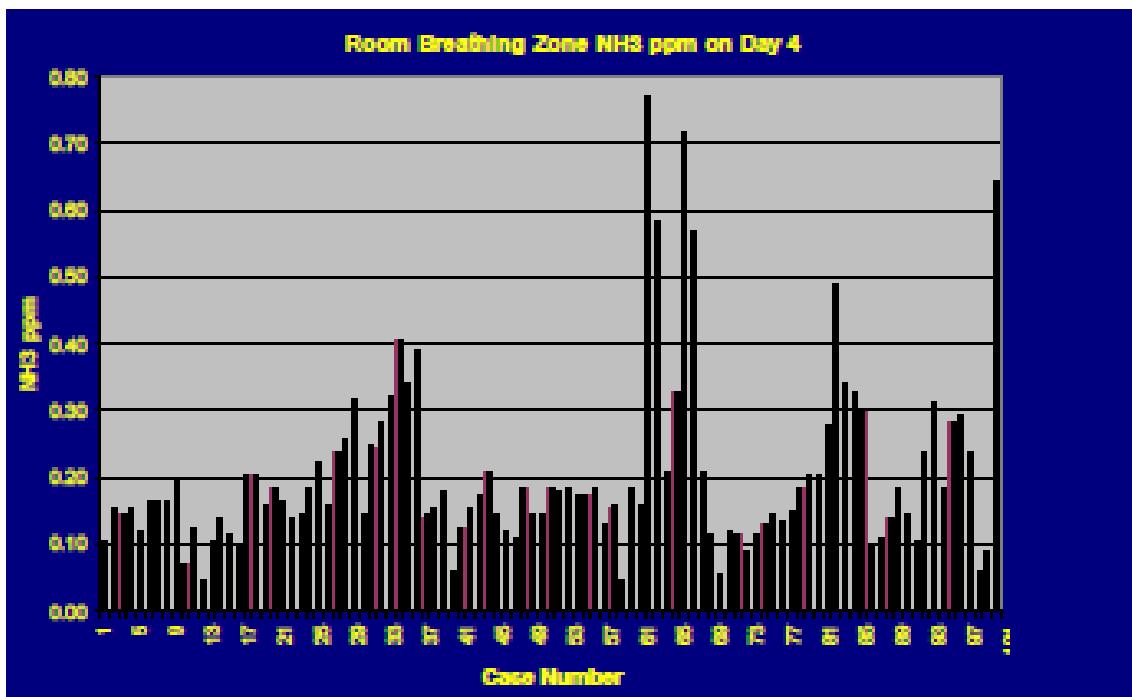


Figure 3.07 Mean Room Breathing Zone NH₃ Concentration on Day 4

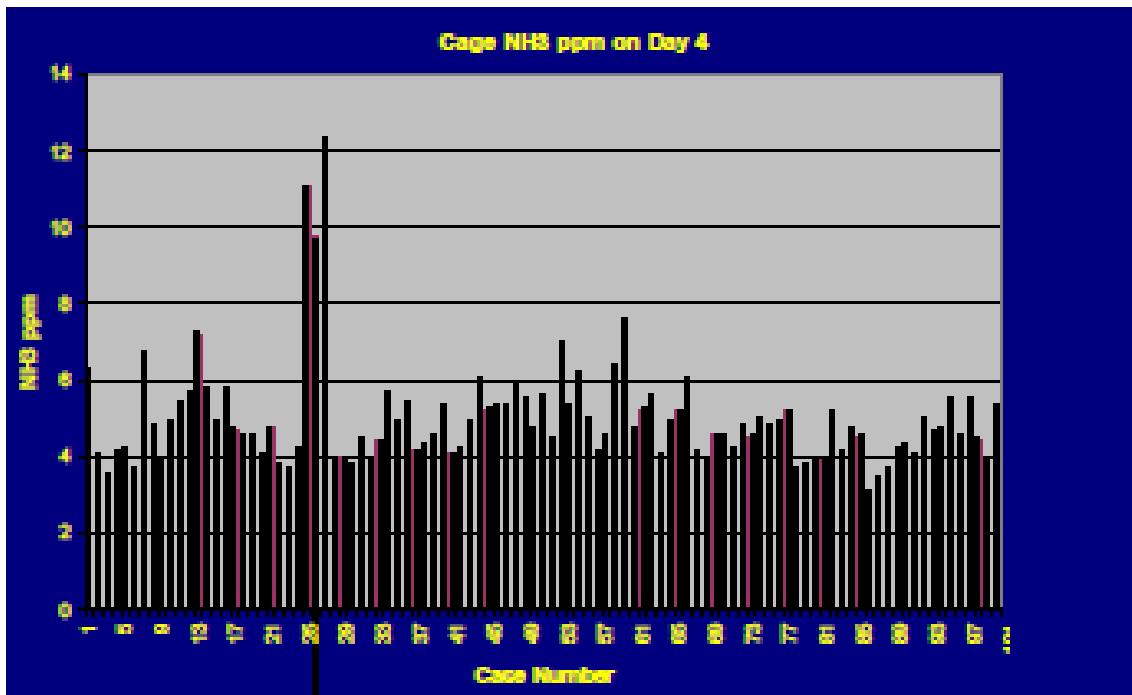


Figure 3.08 Mean Cage NH₃ Concentration on Day 4

Before the detailed comparison of the room configurations, which follows this section, a few general remarks on the results are appropriate.

The ventilation in the rooms was designed to produce 22.2 °C (72.0 °F) at the exhausts in the room (except for cases 99-101). This leads to the room and cage temperatures that do not vary greatly. The variation that does occur seems to be mostly due to temperature stratification in the rooms (i.e., the temperature rises towards the ceiling) in combination with the exhaust position. A low level exhaust means that the design temperature of 22.2 °C (72.0 °F) is the “lowest” in the room whereas a high level exhaust means the temperature should be below 22.2 °C (72.0 °F) in the room.

The CO₂ concentrations are a simple indicator of the ventilation in the room and cages. High values indicate poor ventilation. Good ventilation of the cages can lead to higher values in the room space.

The NH₃ concentration data are more complex measures of the ventilation as they also depend on the relative humidity in the cages, which is also dependent on the temperature. Therefore, poor ventilation of cages at a high temperature and low humidity may produce low NH₃ concentrations.

In making comparisons among the values shown for the cages on the charts, it is important to consider if the differences in the mean values (the average for all cages) is statistically significant. The ANOVA test (see section 6) can be used to determine significant differences. This test was run for several pairs of datasets. In each case the differences were found to be significant, except when the means were actually identical. Please note that comparing 101 datasets with each other for 4 data values produces more than 40,000 tests. This seems to be a result of having 210 or 420 cages in the rooms. Each one appears as a sampling point for the test. With so many samples the test becomes very sensitive and even small variations in means are statistically significant.

3.1.1 *Supply Type and Exhaust Position*

Cases 1 to 9 allow an easy comparison of the effect of Supply type and exhaust position. Cases 1 (the basecase) to 3 had a radial diffuser supply with ceiling, high level (on side walls) and low level (on side walls) exhausts, respectively. Cases 4 to 6 used a slot diffuser, and cases 7 to 9 a low induction diffuser with the same exhaust configurations.

Figures 3.09 to 3.16 show three-dimensional bar charts comparing temperature, CO₂, NH₃, and relative humidity for both the cages and scientists’ breathing zone in the center of the room.

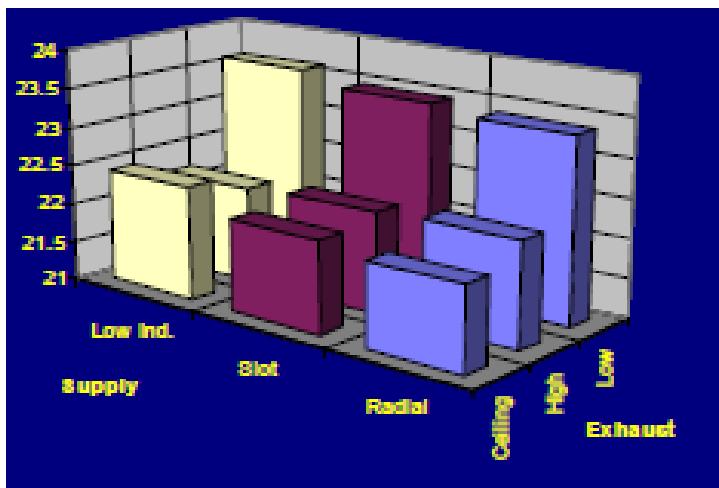


Figure 3.09 Comparison of Mean Cage Temperatures (°C)

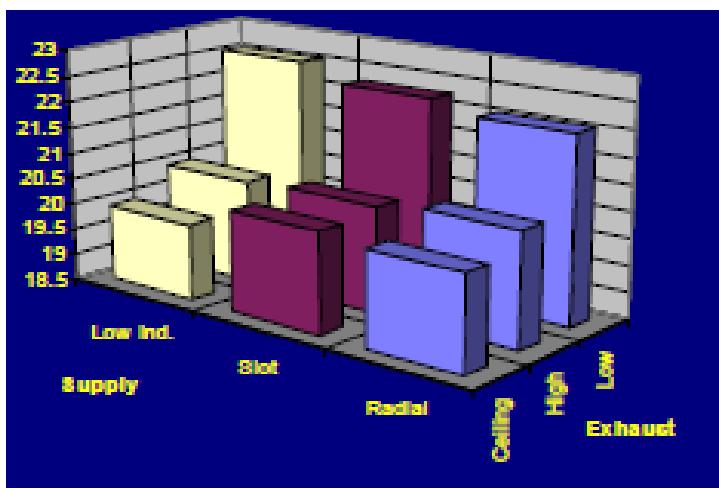


Figure 3.10 Comparison of Room Breathing Zone Temperatures (°C)

The higher temperatures, about 2 °C (4 °F) produced in both the cages and breathing zone in the low level exhaust runs indicates this exhaust location is less efficient in cooling the room compared with the high and ceiling level.

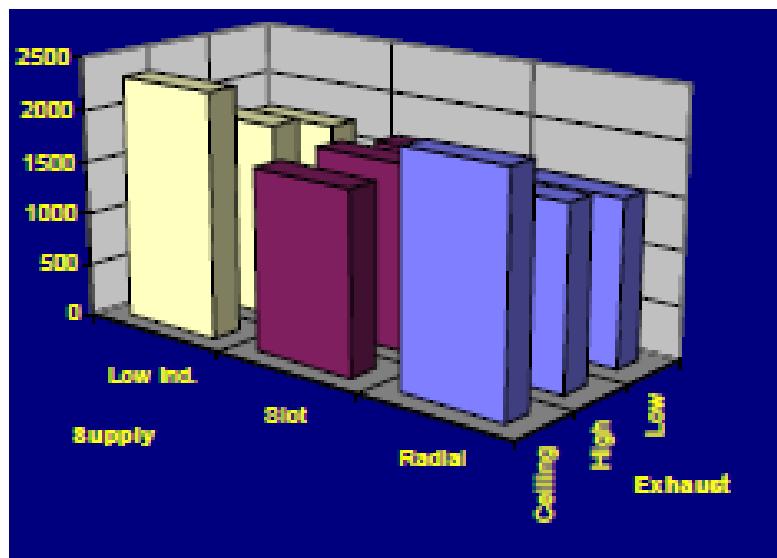


Figure 3.11 Comparison of Mean Cage CO_2 Concentration (ppm)

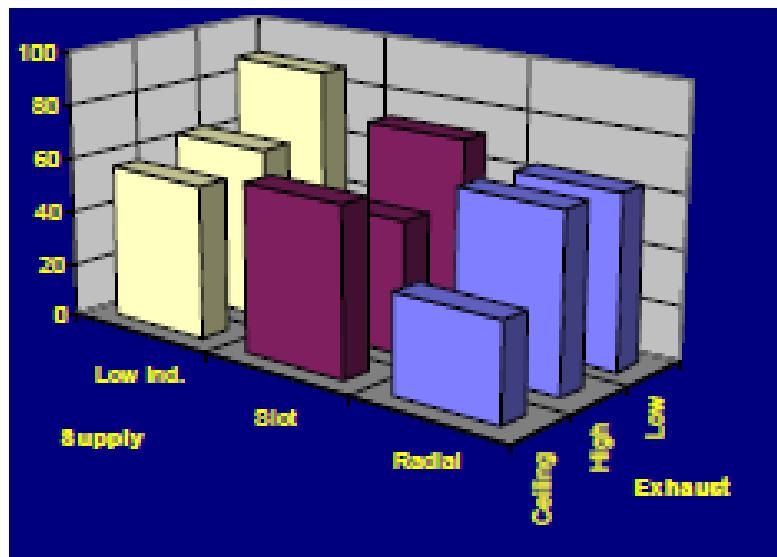


Figure 3.12 Comparison of Room Breathing Zone CO_2 Concentration (ppm)

The lower values of CO_2 concentration in the cages for the low level exhaust (up to 27 percent for the radial diffuser, 4 percent for the slot diffuser and 25 percent for the low induction diffuser) indicate that the cages are better ventilated in this situation. The room values show the best ventilation occurs with a radial diffuser and ceiling level exhausts.

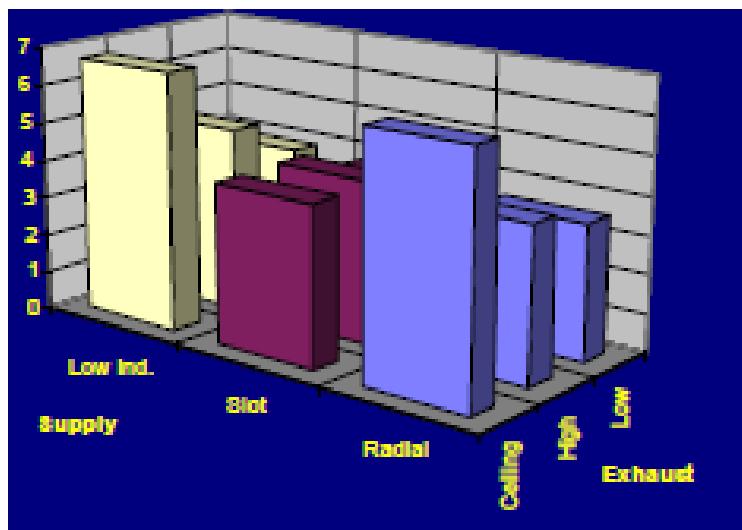


Figure 3.13 Comparison of Mean Cage NH_3 Concentration (ppm)

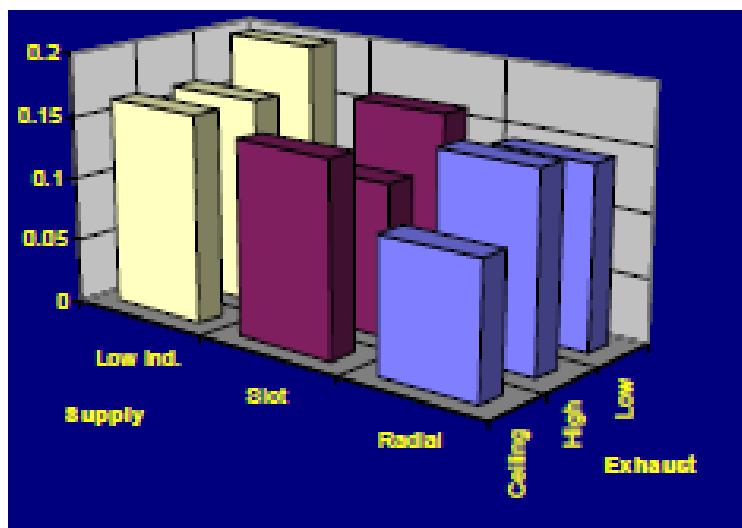


Figure 3.14 Comparison of Room Breathing Zone NH_3 Concentration (ppm)

The cage NH_3 concentrations show a similar pattern to the CO_2 concentrations. The variations are, however, somewhat larger as the higher temperatures in the low level exhaust cases reduce the relative humidity in the cages and reduce the rate of NH_3 generation, which leads to lower concentrations.

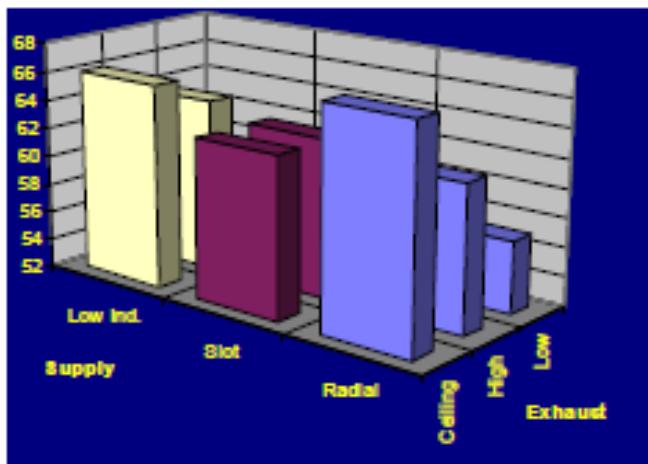


Figure 3.15 Comparison of Mean Cage Relative Humidity (percent)

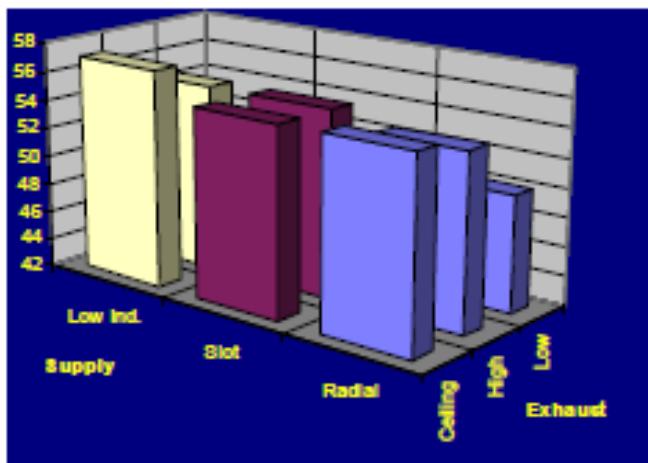


Figure 3.16 Comparison of Mean Breathing Zone Relative Humidity (percent)

Lower humidities in the low level exhaust cases are mainly due to the higher temperatures.

Two features are quickly apparent from these cases:

low level exhausts produce higher temperatures in the room and cages; and

low level exhausts produce the best in-cage ventilation (lowest CO₂ concentrations).

The low CO₂ concentrations seem to be due to the higher flow around the cages. Figures 3.17 and 3.18 show velocity vectors in a slice through the radial supply and the cage racks. For the ceiling level exhaust case (figure 3.17) the velocity vectors are barely visible around the cages, indicating very low flow. In figure 3.18 the low level exhausts case shows much larger velocity vectors representing much greater flow around the cages. This extra flow clearly helps ventilate the cages.

The ceiling level exhausts produce the lowest levels of CO₂ for the radial and low induction diffusers in the room breathing zone. This appears to be caused by the main airflow going through the cages towards the side walls at this height, whereas in the other cases there is more air coming from the side walls into the central region. This can be seen in figures 3.17 and 3.18 as well as in figures 3.19 and 3.20, which show the distribution of CO₂ concentration for the radial diffuser and ceiling and low level exhausts.

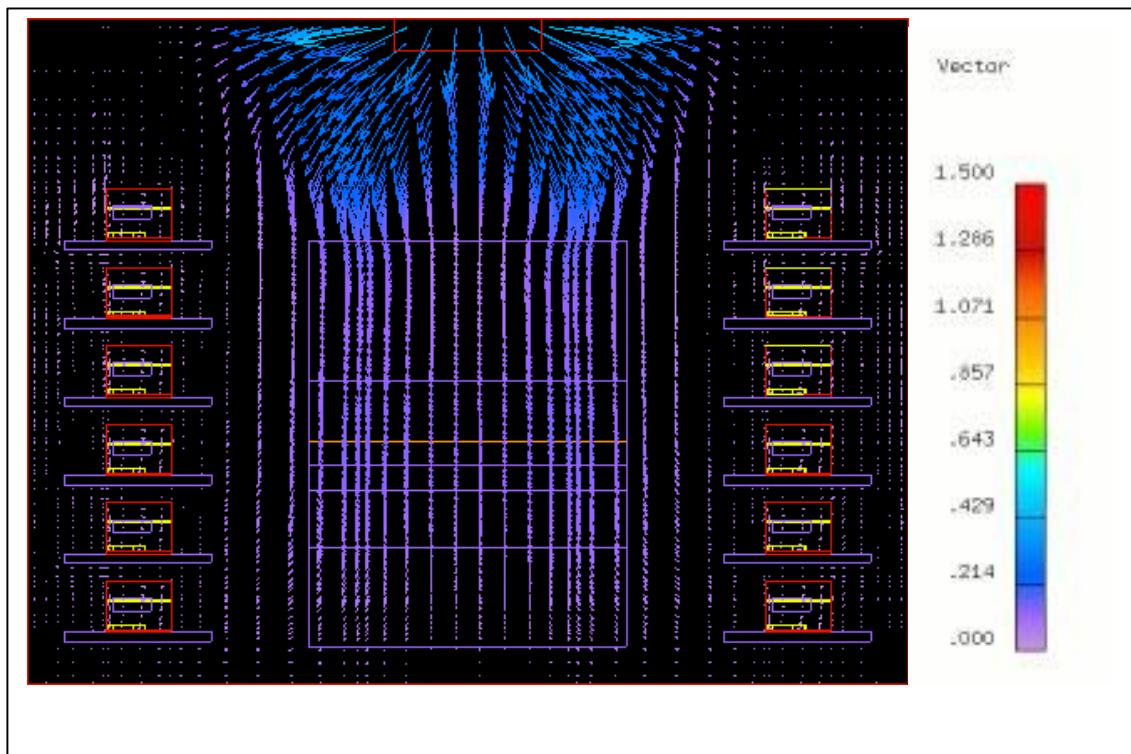


Figure 3.17 Velocity Vectors through the Radial Diffuser with Ceiling Exhausts (basecase)

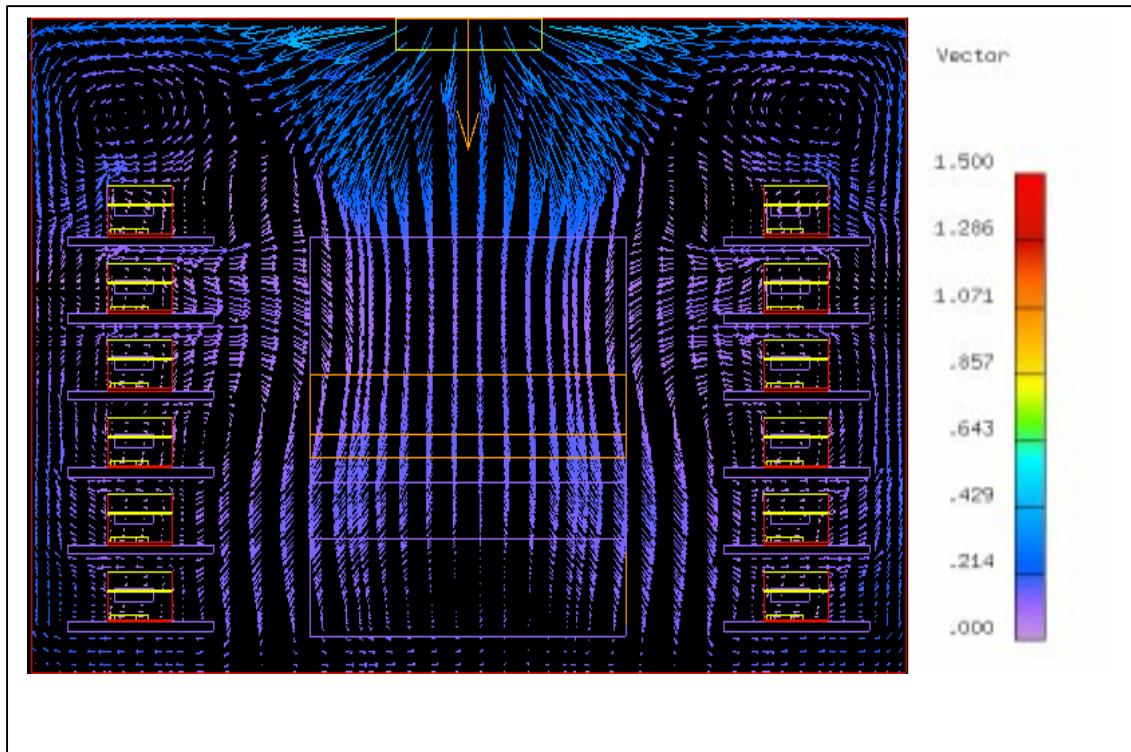


Figure 3.18 Velocity Vectors through the Radial Diffuser with Low Level Exhausts (Case3)

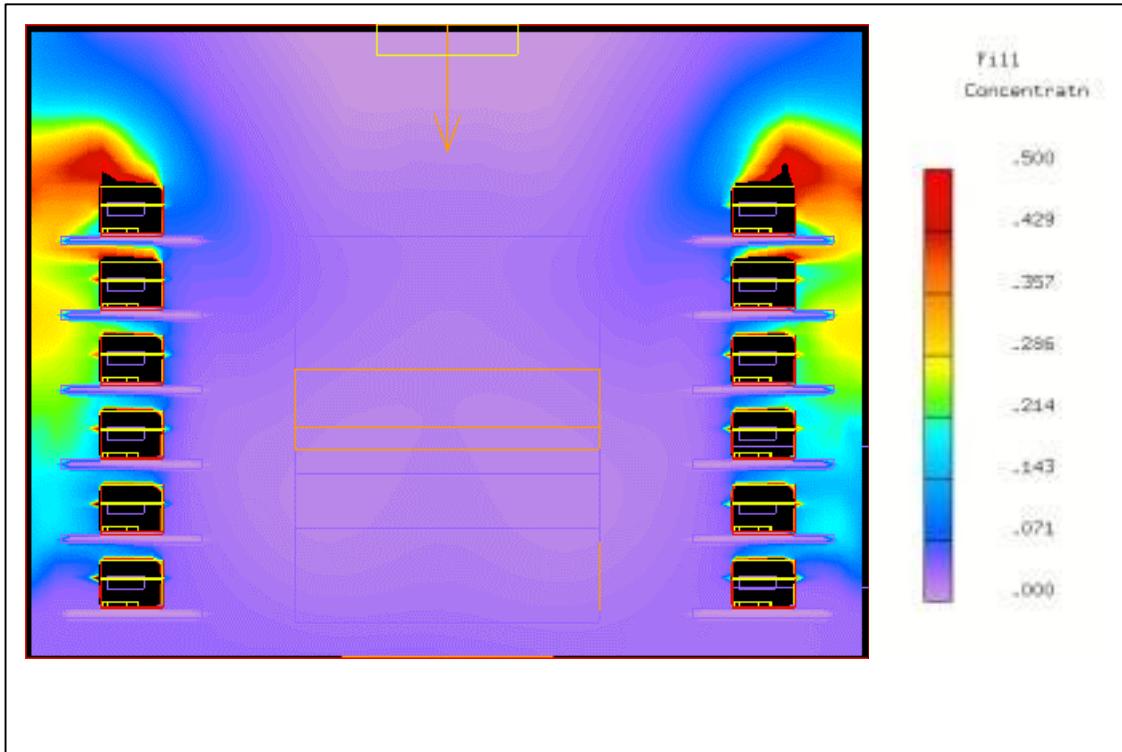


Figure 3.19 CO₂ Distribution (g/kg) Radial Diffuser with Ceiling Exhausts (basecase)

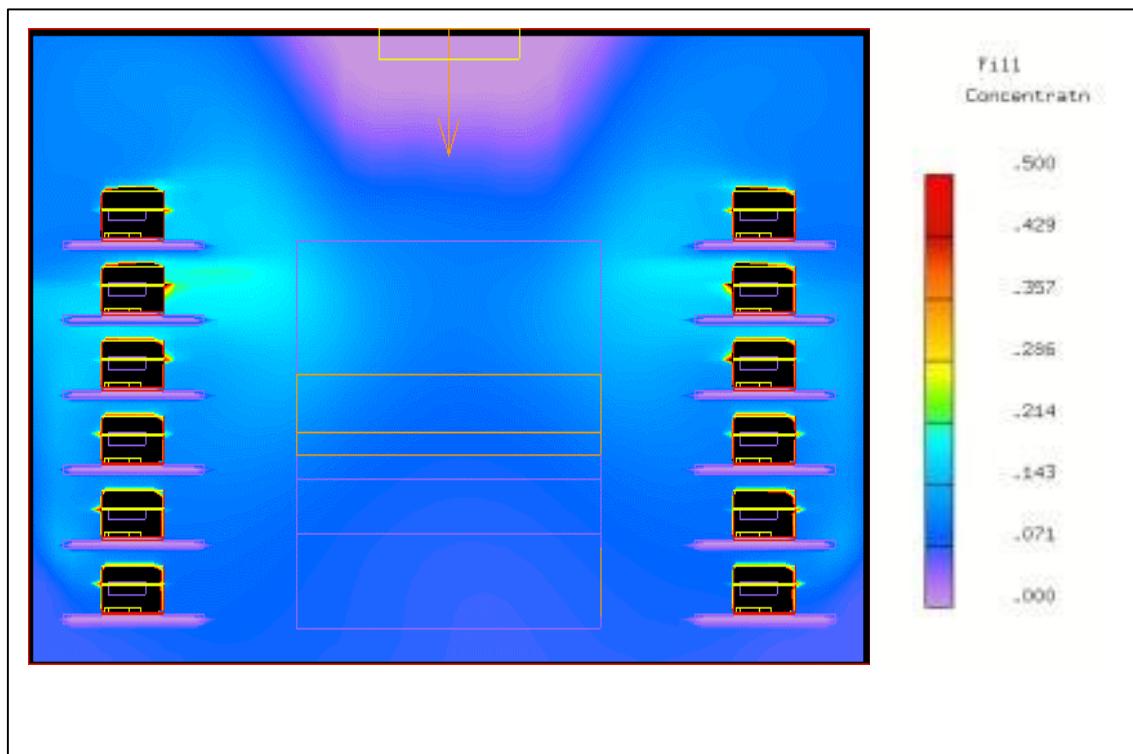


Figure 3.20 CO₂ Distribution (g/kg) Radial Diffuser with Low Level Exhausts (Case3)

Figures 3.21 and 3.22 show slices through the racks of cages for the radial diffuser with ceiling and low level exhausts. The low level exhausts clearly show lower CO₂ concentrations within the cages with less orange/red and more blue/green coloration. The variation in concentration is similar in both cases, with the highest values on the left and right edges of the three rack wall, and slightly lower concentrations in the center and on the tops of most of the racks.

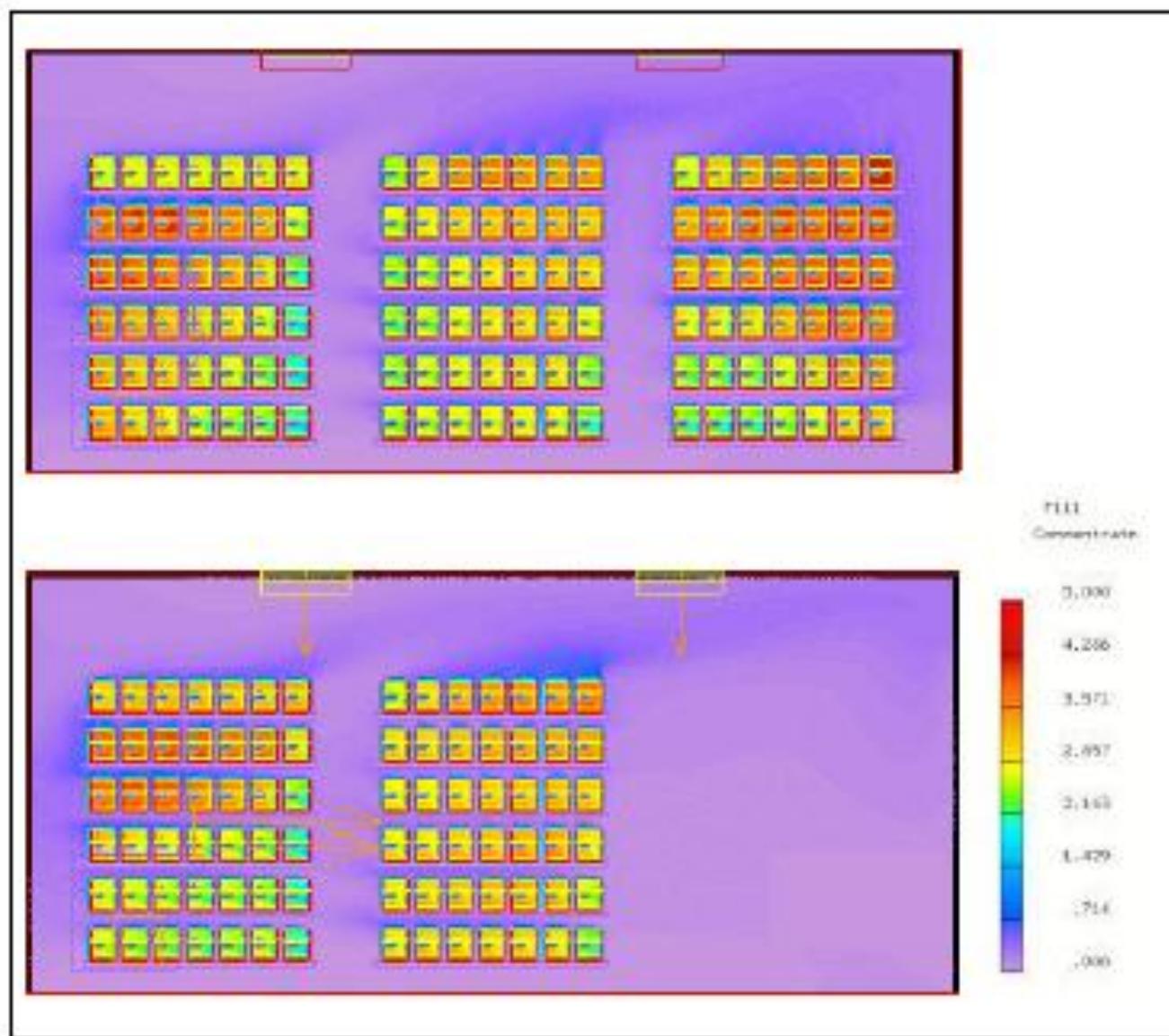


Figure 3.21 CO₂ Concentration (g/kg), Radial Diffuser with Ceiling Exhaust (basecase)

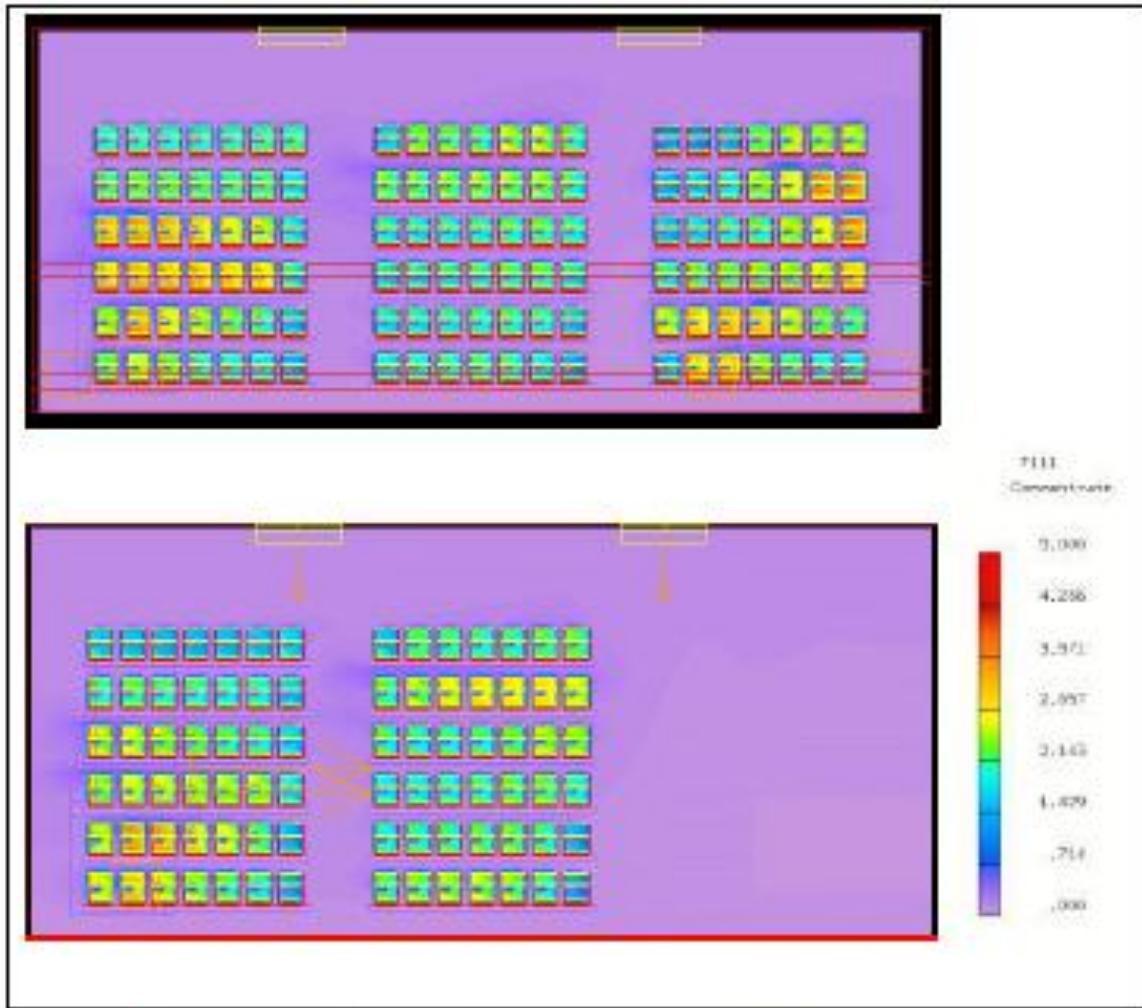


Figure 3.22 CO₂ Concentration (g/kg), Radial Diffuser with Low Level Exhaust (Case3)

The slot diffuser seems least sensitive to exhaust position. This is probably due to the slot diffuser creating much higher entrainment and mixing due to the higher supply air velocity and increased jet area.

The increase in temperature from the lower room ventilation efficiency, apparent in both the cages and the room for the low level exhausts, helps to keep the cage humidity levels low and reduces the NH₃ production.

Further variation in exhaust number and position was investigated in cases 37 to 42, 69 to 75 and 79 to 84. Examination of the data for these runs shows no obvious pattern emerging in cage and room ventilation. Case 40 (radial supply and four ceiling exhausts in the corners) seems to produce particularly low room breathing zone CO₂ and NH₃ concentrations, improving on the basecase values. However the other cases with four ceiling exhausts do not seem significantly better than the two ceiling exhaust cases.

3.1.2 Air Change Rate

Figures 3.23 to 3.28 show comparisons of temperature, CO₂ and NH₃ concentrations for both the cages and scientists' breathing zone for airflow rates between 5ACH and 20ACH. The plots show results for single density racks (42 cages) parallel to the walls (cases 9, 28-30) and double density racks (84 cages, cases 33, 62-64) perpendicular to the walls as well as a variation in change station design (84 cages, cases 65-68). All cases have low induction supplies and low level exhausts.

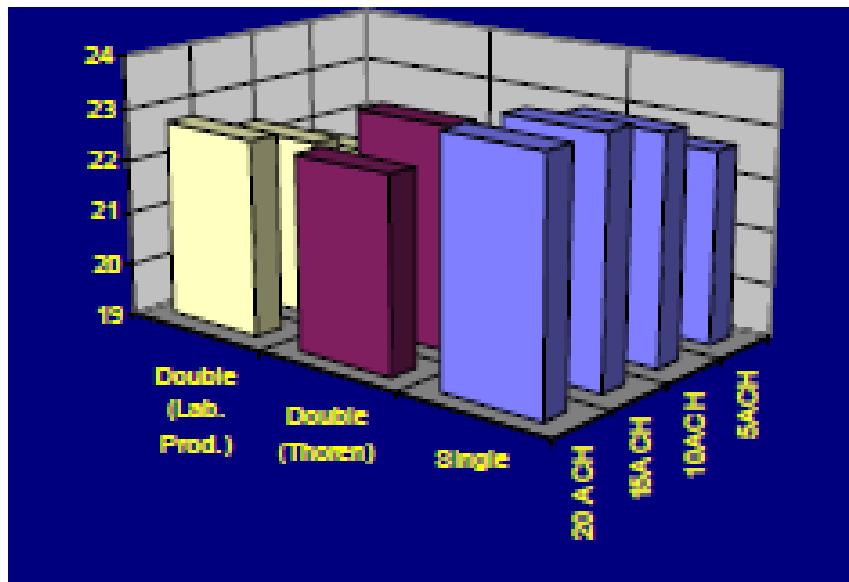


Figure 3.13 Comparison of Mean Cage Temperature (°C)

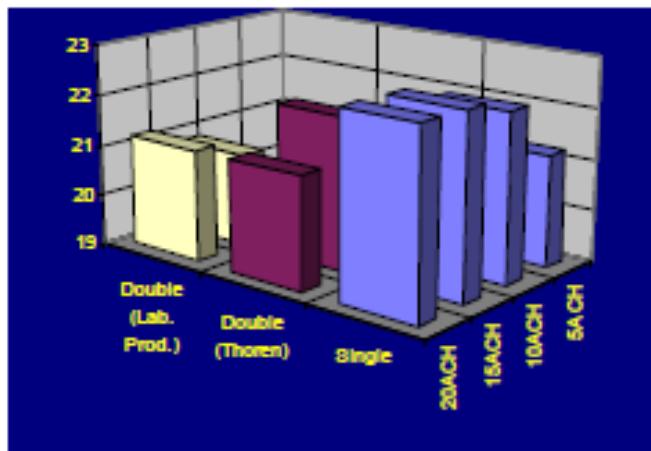


Figure 3.24 Comparison of Room Breathing Zone Temperature (°C)

The cage temperatures vary very little in comparison with the variation in supply temperature (from 19.8 °C (68 °F) to 6.6 °C (44 °F)) and follow the trends shown in the breathing zone temperature. The slightly lower supply temperatures in the double density cases (more mice produce more heat to be extracted) lead to a small reduction in both room and cage temperatures compared with the single density racks.

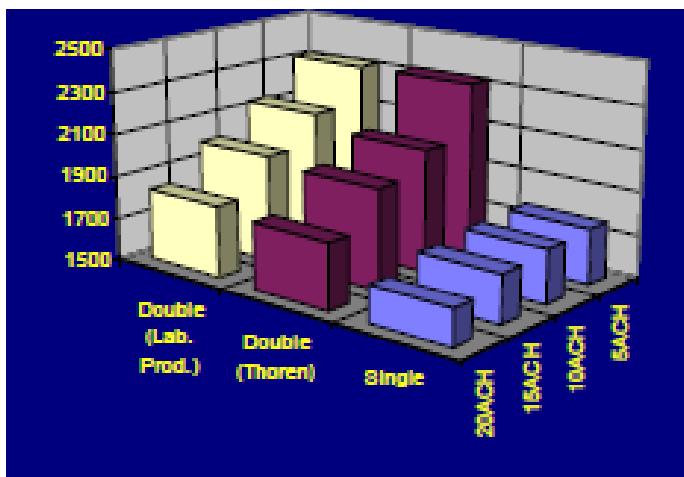


Figure 3.25 Comparison of Mean Cage CO₂ Concentrations (ppm)

Increasing the room ventilation rate does not have a large effect on the cage ventilation. Increasing the supply flow rate from 5 ACH to 20 ACH for single density racks parallel to the

walls reduces the CO₂ concentration from 1,764 ppm to 1,667 ppm, a reduction of only six percent. For the double density racks perpendicular to the walls the reduction is larger, but still only from about 2,300 ppm to 1,800 ppm (about 20 percent).

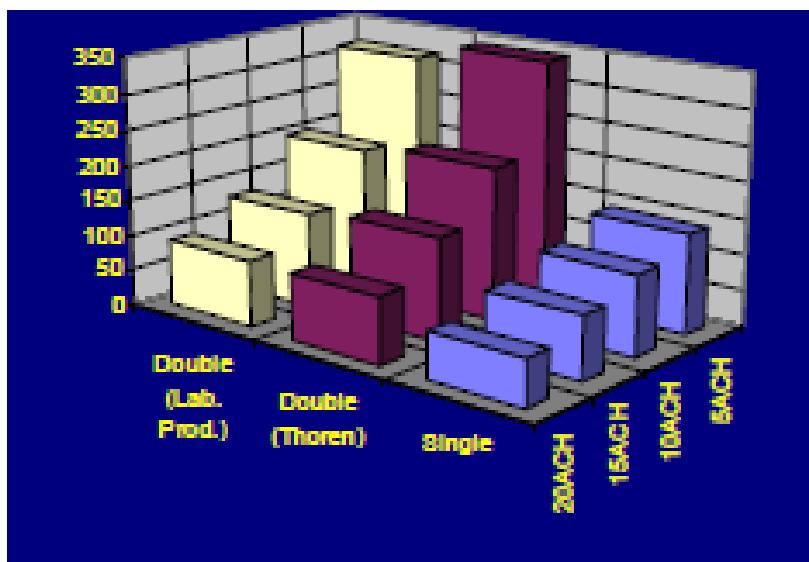


Figure 3.26 Comparison of Room Breathing Zone CO₂ Concentrations (ppm)

Increasing the room ventilation rate has a continuous beneficial effect on the room breathing zone ventilation (as measured by CO₂ and ammonia concentrations). For the single density racks parallel to the walls increasing the supply flow rate from 5 ACH to 20 ACH reduces the breathing zone CO₂ concentration from 140 ppm to 63 ppm, a decrease of 55 percent. For the double density racks perpendicular to the walls the reduction is even more dramatic, from over 300 ppm to 93 ppm (over 70 percent reduction) when the flow rate is increased from 5 ACH to 20 ACH. However, the “high” values of CO₂ concentration, of about 300 ppm above the background levels, are still significantly too low. The American Conference of Governmental Industrial Hygienists (ACGIH) recommends a threshold limit value (TLV), time weighted average (TWA) of 5,000 ppm (9,000 mg/m³) for carbon dioxide. ACGIH also recommended a Short Term Exposure Limit (STEL) of 30,000 ppm (54,000 mg/m³).

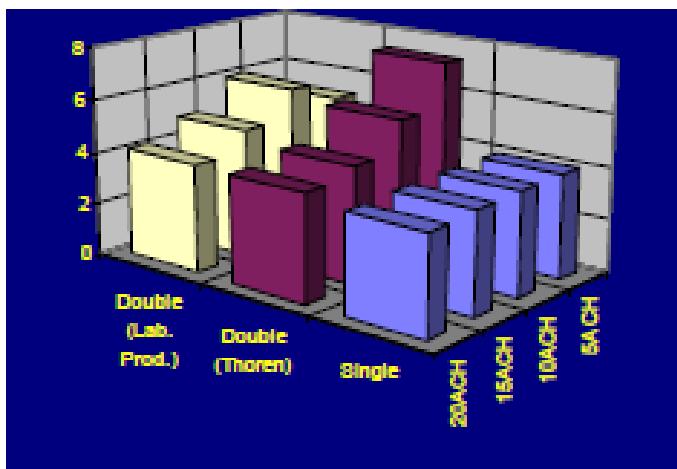


Figure 3.27 Comparison of Mean Cage NH₃ Concentrations (ppm)

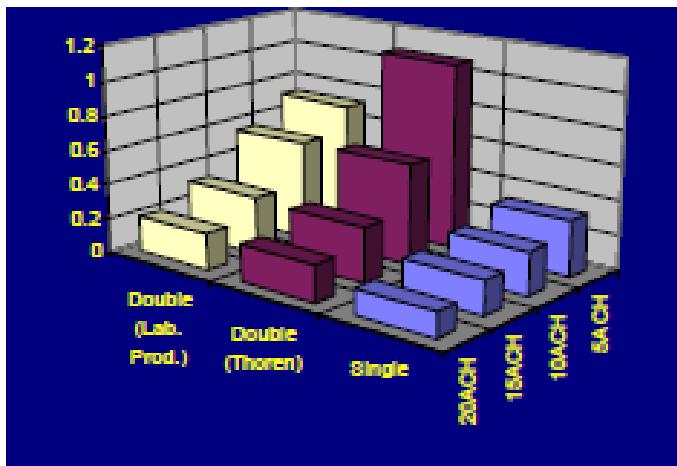


Figure 3.28 Comparison of Mean Breathing Zone NH₃ Concentrations (ppm)

The NH₃ concentrations follow the trends shown by the CO₂ concentrations. The 5 ACH NH₃ results are not directly comparable with those for the other flow rates. This is due to the extremely low supply discharge temperature 6.6 °C (44 °F) required to extract the heat produced by the mice and the change station, which required the moisture content of the air to be reduced compared to the other flow rates. The standard value used in the simulations represented well over 100 percent humidity. It is also recognised that this low temperature is difficult, if not impossible, to achieve in commercial heating and ventilation systems.

The results do indicate that the cages are not significantly better ventilated at higher flow rates. The rooms are better ventilated up to 20 ACH as would be expected because there is more fresh air available to dilute the gases produced by the mice.

The animal loading in the room is clearly significant. The 5 ACH supply rate in the room with single density cage racks (case 29) produces less than 50 percent of the room CO₂ concentration compared with the 5 ACH with the double density racks (cases 62 and 66). Since 10 ACH seems acceptable for day 4 NH₃ concentration in the cages of the double density rooms, and 5 ACH is acceptable for NH₃ concentrations in the cages of single density rooms, the airflow required in the room is best at 0.85 cfm (4.01e-4 m³/s) per cage of five mice or 100g body weight of mice (see also section 3.2 below).

3.1.3 Change Station Design and Status

Cases 10 to 15 were run with the change station switched off and no heat generation or recirculated air. These should be compared with cases 1, 3, 4, 6, 7, and 9. Figures 3.29 to 3.32 show comparisons of CO₂ and NH₃ concentrations for the three supply diffusers with ceiling level exhausts and the Thoren change station in operation (on) and also with it present but not operating (off).

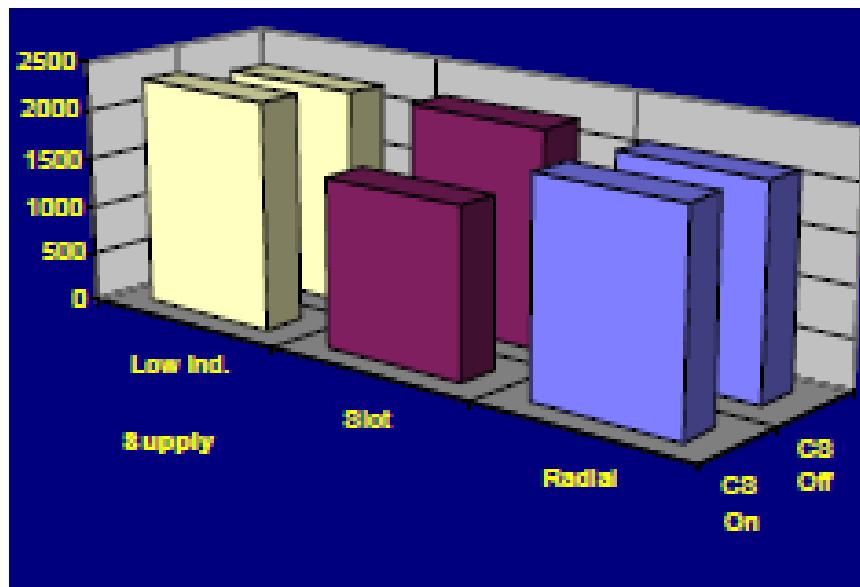


Figure 3.29 Comparison of Mean Cage CO₂ Concentrations (ppm)

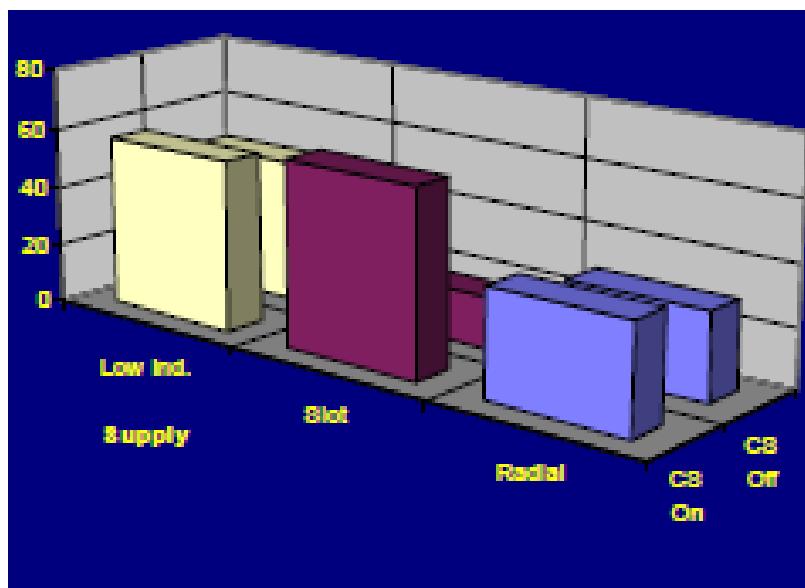


Figure 3.30 Comparison of Mean Breathing Zone CO_2 Concentrations (ppm)

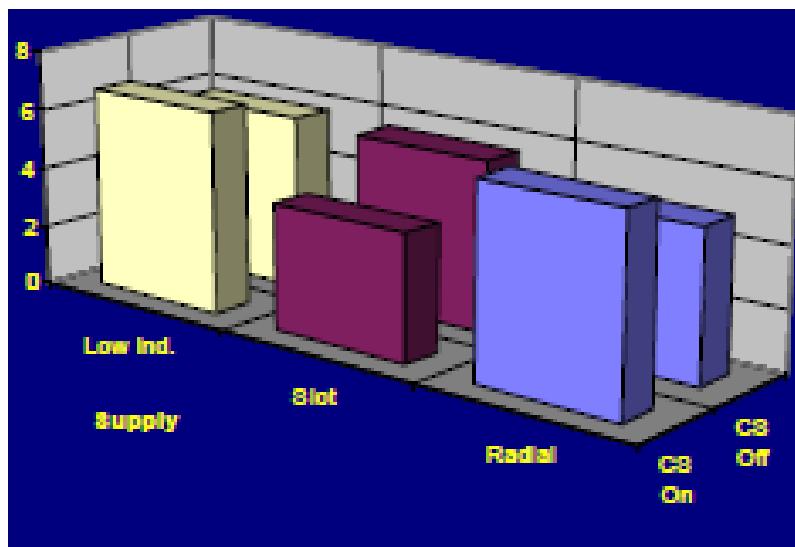


Figure 3.31 Comparison of Mean Cage NH_3 Concentrations (ppm)

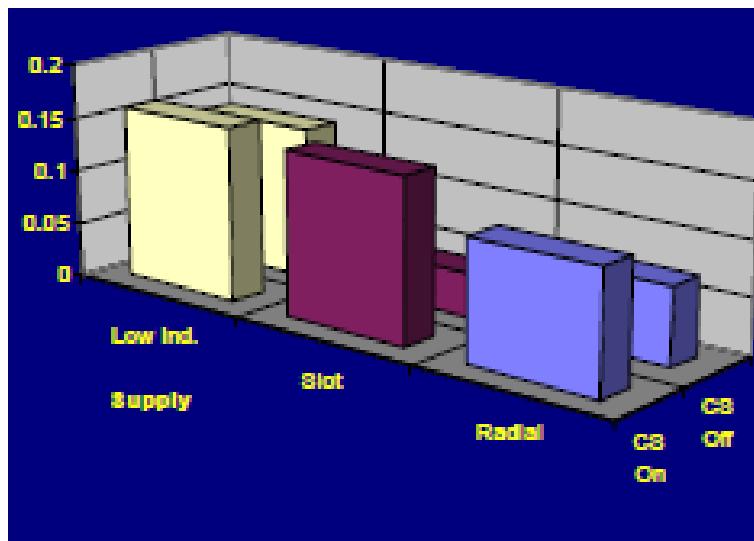


Figure 3.32 Comparison of Mean Breathing Zone NH₃ Concentrations (ppm)

Switching off the change station seems to decrease slightly the CO₂ and NH₃ concentrations in both the cages and the room for the radial and low induction supplies. The slot diffuser shows a small increase in both CO₂ and NH₃ concentrations in the cages, although the room values show a large decrease. This indicates the difficulty in making generalizations because the effect of making a change is very dependent on the case under consideration.

The change station produces a strong airflow upwards when active (see figure 3.33), which acts to mix dirty air from the cages with the fresh air from the supplies.

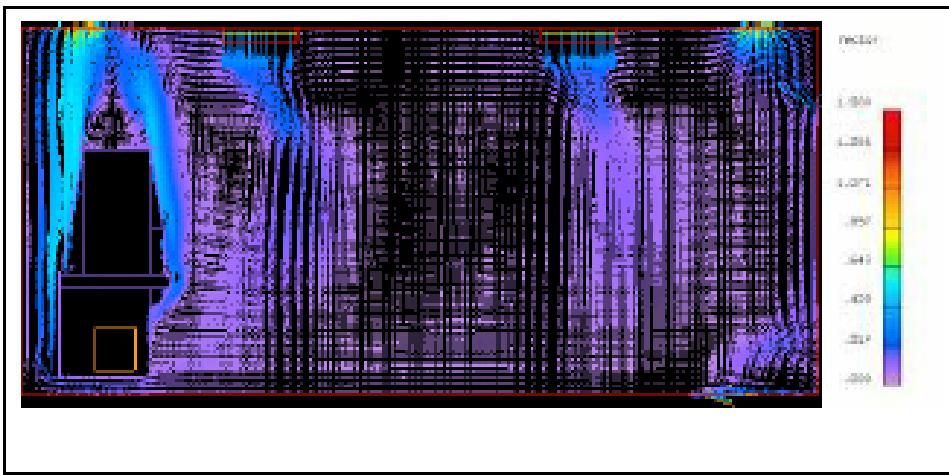


Figure 3.33 Velocity Vectors on the Centerline for the Basecase Showing the Strong Upward Flow from the Change Station

Cases 53 to 61 were run with an alternative change station design that had similar heat dissipation but a higher amount of recirculated air. This design seems to produce results very similar to those of the original change station.

It is interesting that two of the best performances for the room breathing zone CO₂ and NH₃ concentrations come out of this group of tests. Case 12 (slot supply, ceiling exhaust, change station off) and case 59 (slot supply, low level exhaust, alternative change station) produce the lowest CO₂ and NH₃ concentrations in the room. That there is no obvious link between these cases, and since other slot supply cases do not appear to be so good, this information serves to confirm that such complex airflows take place in animal rooms, it is difficult to predict how they will perform without detailed analysis.

3.1.4 Pressurization of Room relative to Corridor

Cases 16 to 18 were run with positive pressurization in the room instead of negative, with 100cfm (4.72e-2 m³/s) air leaving rather than entering the room via the door. These cases should be compared with cases 1, 4 and 7, which are all cases with ceiling exhausts. Cases 45 to 47 varied the amount of air flowing in or out (50cfm in, 0cfm, and 50cfm out) of the door cracks and should be compared with cases 1 and 16.

Figures 3.34 to 3.37 show comparisons of CO₂ and NH₃ concentrations for different room pressurizations.

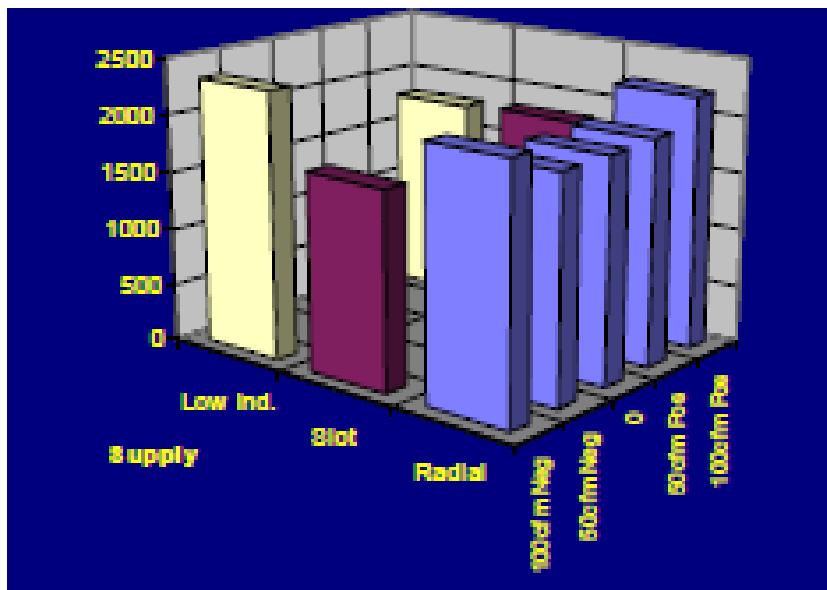


Figure 3.34 Comparison of Mean Cage CO_2 Concentrations (ppm)

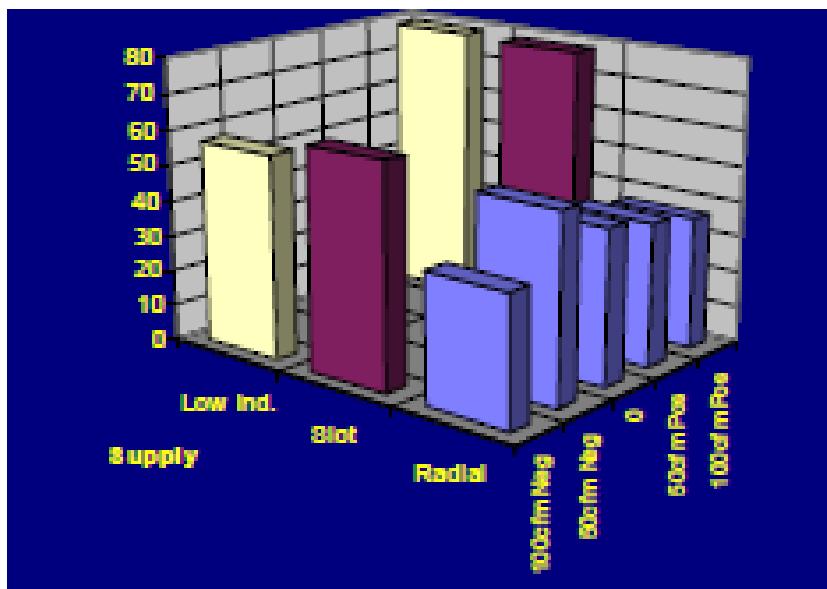


Figure 3.35 Comparison of Mean Breathing Zone CO_2 Concentrations (ppm)

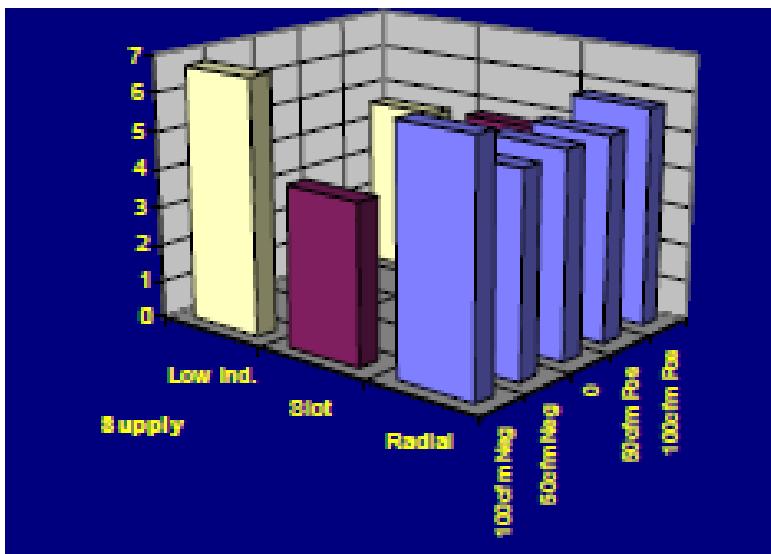


Figure 3.36 Comparison of Mean Cage NH₃ Concentrations (ppm)

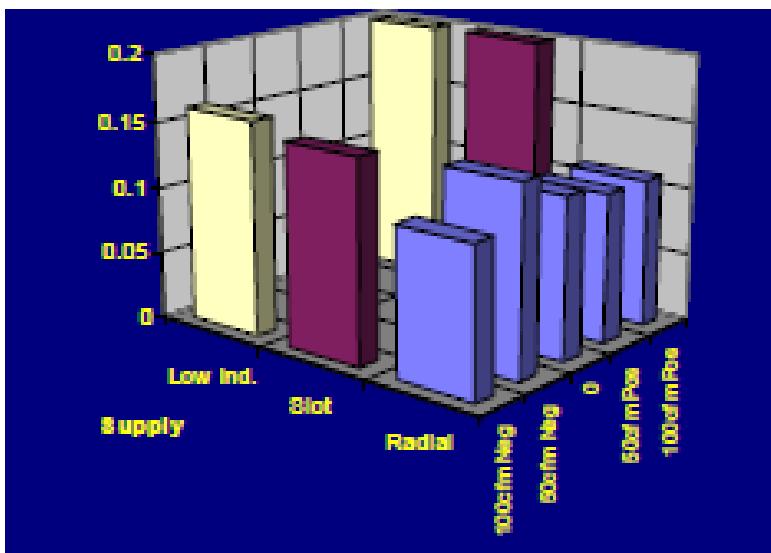


Figure 3.37 Comparison of Mean Breathing Zone NH₃ Concentrations (ppm)

100cfm inflow makeup air (negative pressurization) and 100cfm outflow makeup air (positive pressurization) represents around 18 percent of the supply diffuser flow rate at 15 ACH. Changing the direction of the makeup airflow has different effects on the CO₂ and NH₃ concentrations depending on the diffuser type. The radial diffuser, which was also run at 50 cfm positive and negative as well as neutral 0cfm, shows only small variations in both the room and cages.

The slot diffuser also shows little variation, with a small increase in cage concentrations and slightly larger increases in room concentrations, going from negative to positive pressurization. The low induction diffuser shows increases in room concentration but decreases in cage concentrations.

Again it is difficult to make a general recommendation. The effects seem small and dependant on the actual details of the configuration under study.

3.1.5 *Orientation of Cage Racks in Room and Rack Grouping*

Cases 19 to 24 were run with the five racks positioned perpendicular to the side walls rather than parallel to them. They should be compared with cases 1, 3, 4, 6, 7, and 9. This orientation removes the central open area in the room for the scientists as the racks overlap. However, data for the scientist's breathing zone are still reported although this is somewhat smaller. The analysis excluded a 0.15m (6") space around each cage.

Figures 3.38 to 3.41 show comparisons for the three diffuser types with ceiling level exhausts for single density racks parallel and perpendicular to the walls.

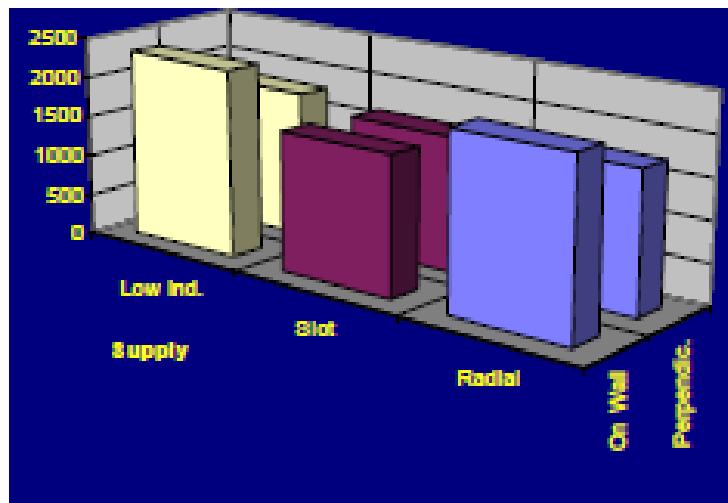


Figure 3.38 Comparison of Mean Cage CO₂ Concentrations (ppm)

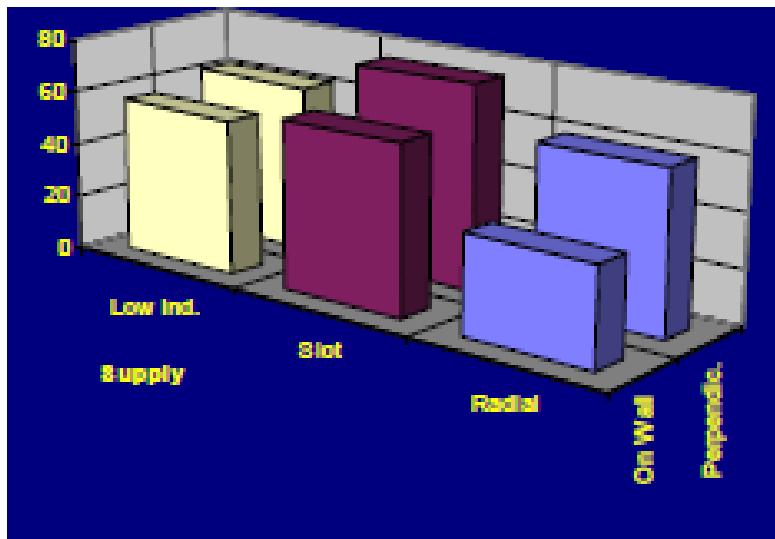


Figure 3.39 Comparison of Mean Breathing Zone CO₂ Concentrations (ppm)

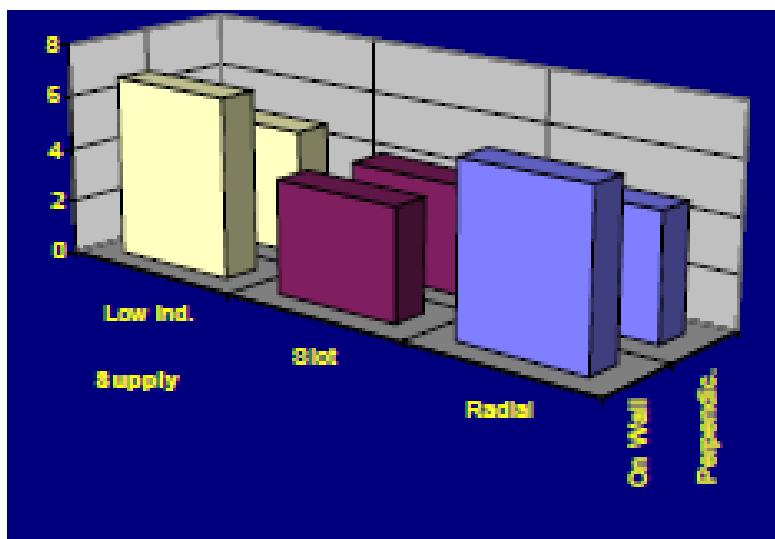


Figure 3.40 Comparison of Mean Cage NH₃ Concentrations (ppm)

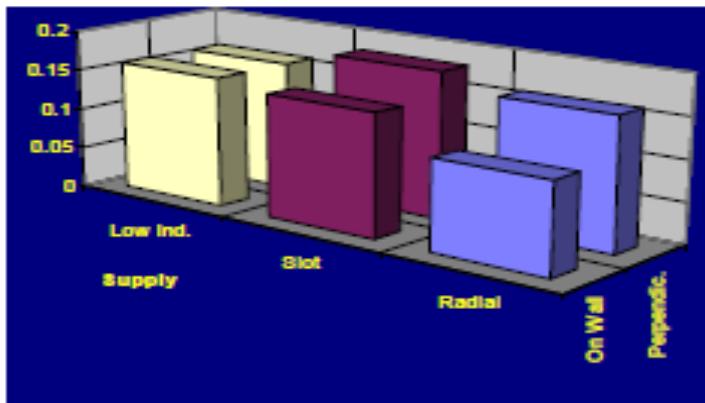


Figure 3.41 Comparison of Mean Breathing Zone NH₃ Concentrations (ppm)

The radial and low induction diffusers show a reduction in cage CO₂ and NH₃ concentrations in the cages with clearly better ventilation through the racks (and cages) in this perpendicular orientation. The in-room breathing zone values show similar or slightly increased CO₂ and NH₃ concentrations.

Cases 48 to 52 were run with different positions for the change station (swapped with particular racks) and cases 90 to 92 were run with all five racks positioned on one wall rather than split two on one wall and three on the other. Again, variations in CO₂ and NH₃ concentrations for both the cages and the room are small.

In conclusion, apart from the improvement in cage ventilation for the radial and low induction diffusers when the racks are perpendicular to the walls, no particular advantage or disadvantage in any orientation or rack layout can be seen.

3.1.6 Density of Cages

Cases 31 to 36 were run with double the number of cages on each rack. This meant a total of 420 cages were present in the room. To provide easy access to all the cages it was necessary to use only rack orientations that were perpendicular to the side wall (i.e., into the room not parallel to the side walls).

Figures 3.42 to 3.45 show comparisons of CO₂ and NH₃ concentrations for the three supply diffuser types with ceiling and low level exhausts.

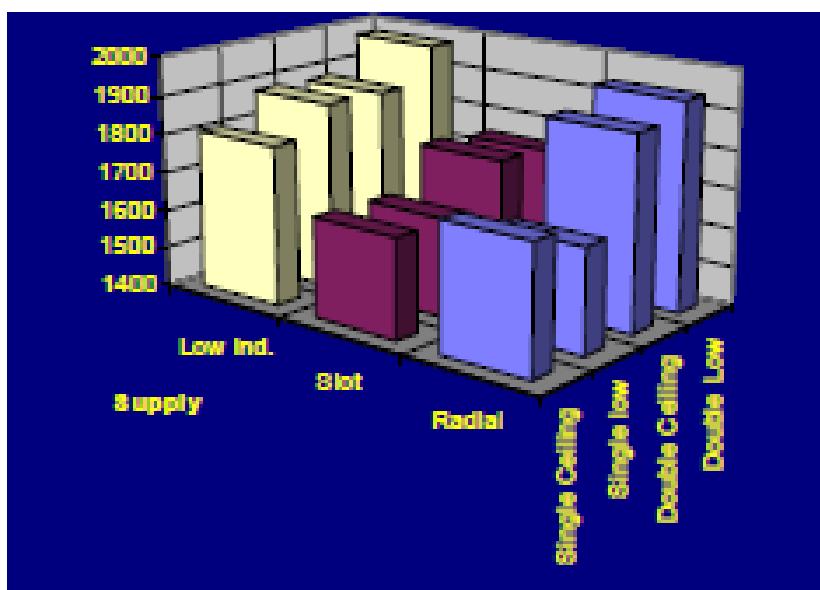


Figure 3.42 Comparison of Mean Cage CO₂ Concentrations (ppm)

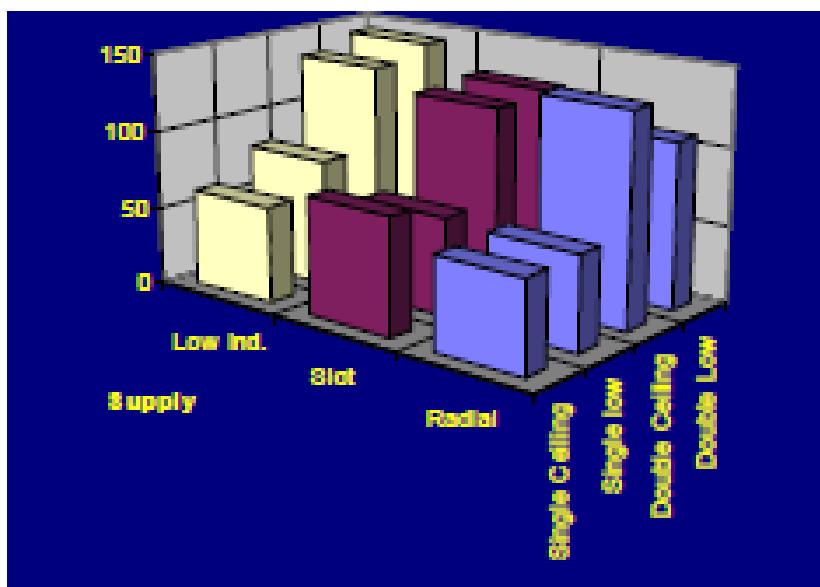


Figure 3.43 Comparison of Mean Breathing Zone CO₂ Concentrations (ppm)

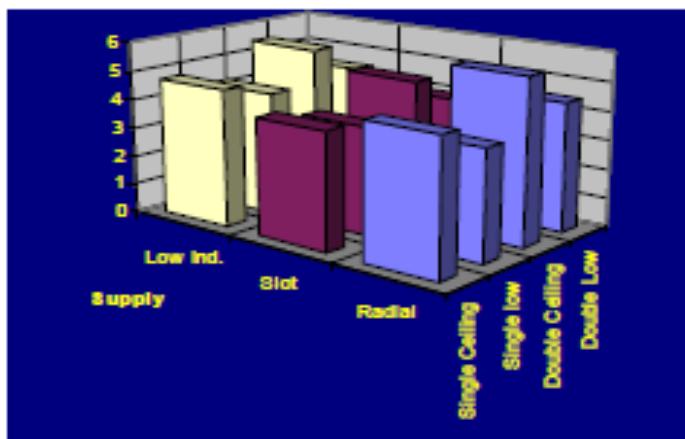


Figure 3.44 Comparison of Mean Cage NH_3 Concentrations (ppm)

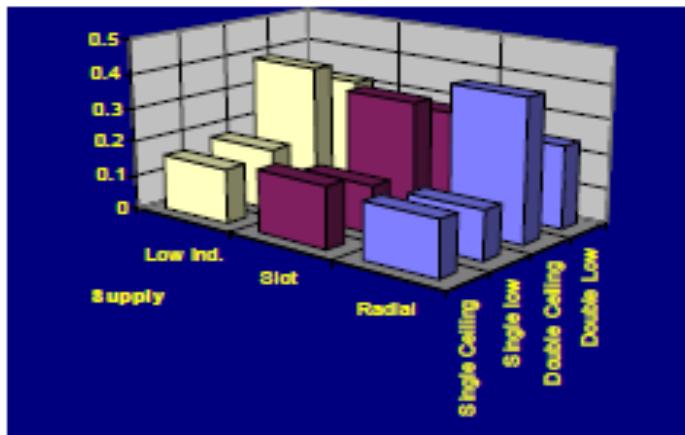


Figure 3.45 Comparison of Mean Breathing Zone NH_3 Concentrations (ppm)

The in-cage values for these runs are not very different from the single density rack. The in-room breathing zone values are much higher. They are about double the CO_2 and NH_3 concentrations of the single density (compare with cases 19 to 24).

Cases 62 to 68 were also double density runs with variation in air change rate. These cases were discussed in section 3.1.2. These cases were the worst, run with 5 ACH producing very high NH_3 concentrations in the scientist's breathing zone.

Cases 87 to 89 were run with a reduced number of cages on each rack (28 instead of 42) for each supply type with low level exhausts. Apart from the slight reduction in room breathing zone CO₂ and NH₃ concentration, no particular changes can be seen. The radial supply seems the best in the room and the low induction the worst, as is the case with the normal racks (42 cages).

3.1.7 Side Cracks of Cages Sealed instead of Open

Where the bonnet filter top sits on the bottom of the microisolator cage the CFD model allowed for an imperfect fit, i.e., air could enter or leave the cage via small cracks. To investigate this effect, three cases were run with sealed cracks, i.e., no air could enter or leave the cages except through the filter.

Cases 25 to 27 were run with sealed cages instead of leaky ones for the three supply types and ceiling exhausts (compare with cases 1, 4 and 7).

Figure 3.46 shows the comparison of in-cage mean temperatures and shows very little change difference between the normal cage model and the fully sealed one.

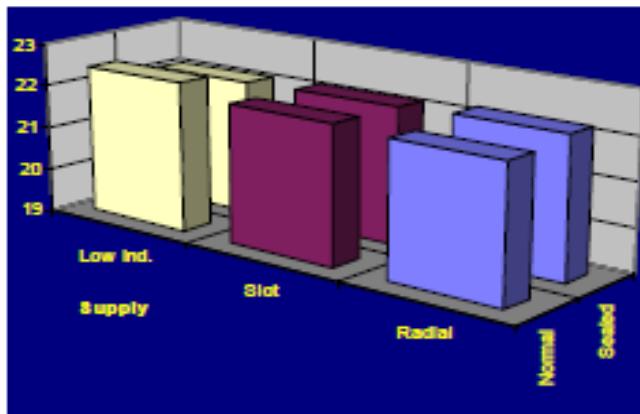


Figure 3.46 Comparison of Mean Cage Temperatures (°C)

Figures 3.47 to 3.50 show comparisons of CO₂ and NH₃ concentrations for the three supply diffuser types with ceiling exhausts for the normal and sealed cage.

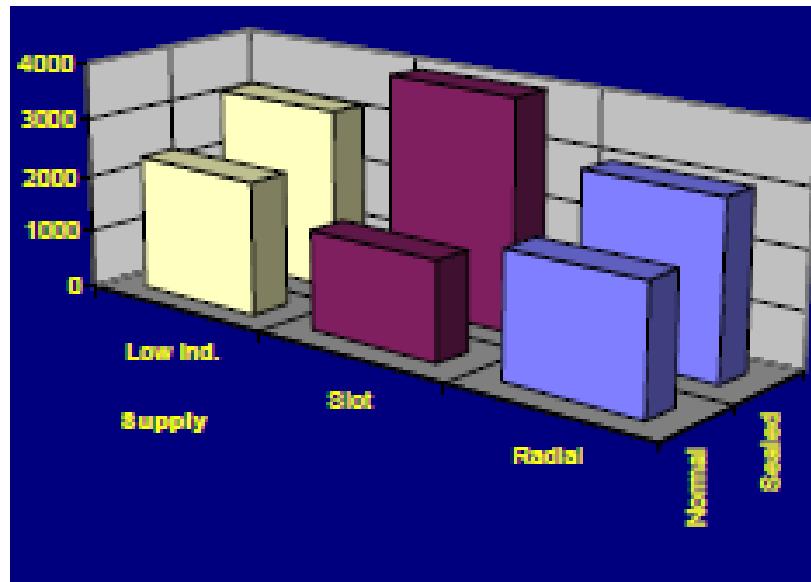


Figure 3.47 Comparison of Mean Cage CO_2 Concentrations (ppm)

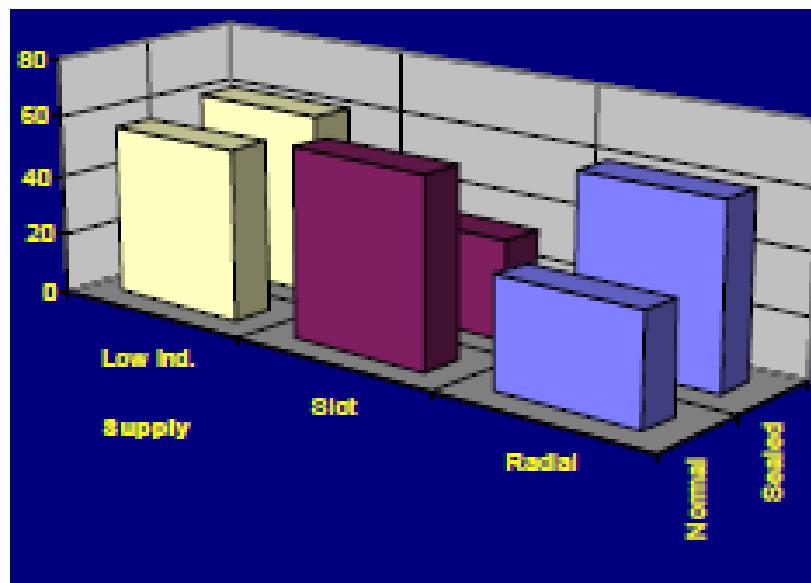


Figure 3.48 Comparison of Mean Breathing Zone CO_2 Concentrations (ppm)

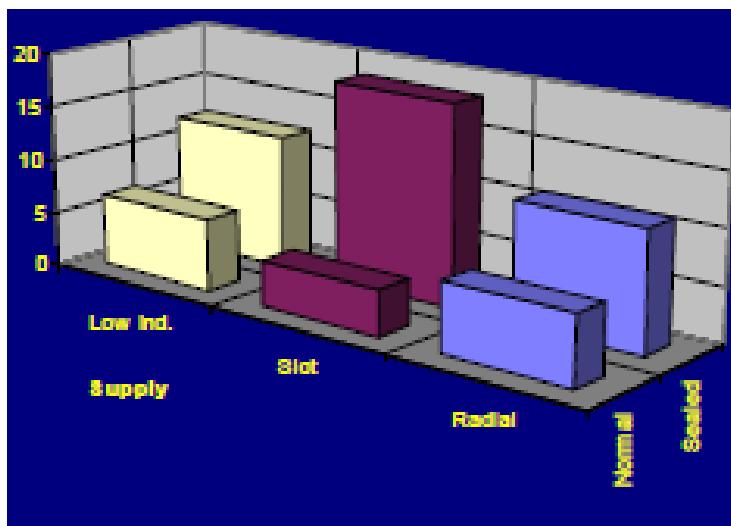


Figure 3.49 Comparison of Mean Cage NH₃ Concentrations (ppm)

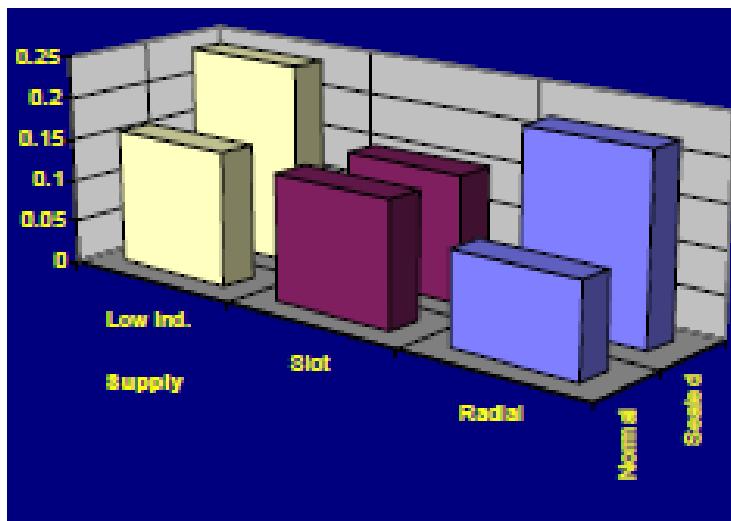


Figure 3.50 Comparison of Mean Breathing Zone NH₃ Concentrations (ppm)

The cages show large increases in both CO₂ and NH₃ concentrations. The room values show little variation in CO₂ concentration but an increase in NH₃ concentration. This is due to the increased cage relative humidities (see figure 3.51) which causes an increased NH₃ generation.

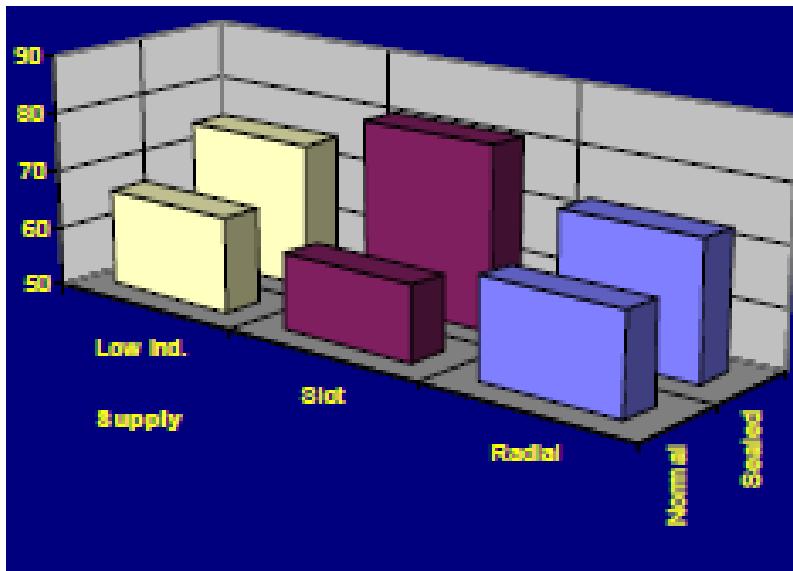


Figure 3.51 Comparison of Mean Cage Relative Humidity (percent)

Although the ventilation of the cages is much worse, which leads to the high concentrations, the temperatures within the cages are not noticeably different. This is partly to be expected, as the CFD model of the mice is a constant temperature model. Even if there was no ventilation of the cages, the temperature in the cage cannot exceed the 30.0 °C (86.0 °F), which is the surface temperature of the mice.

3.1.8 Room Width

Cases 76 to 78 were run with an increased room width 4.26m (14' 0") instead of the original width of 3.66m (12' 0"), with ceiling exhausts for the three supply types. They should be compared with cases 1, 4 and 7. Figures 3.52 to 3.55 show comparisons of CO₂ and NH₃ concentrations.

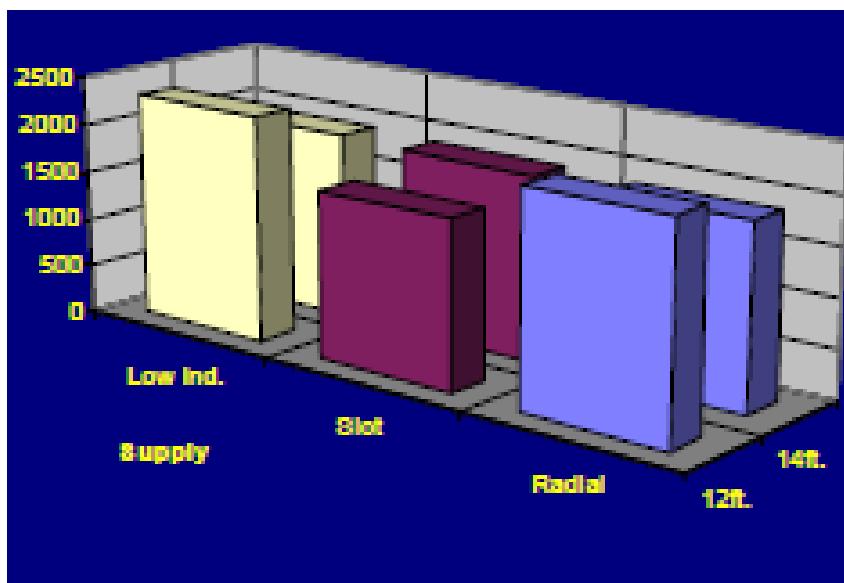


Figure 3.52 Comparison of Mean Cage CO₂ Concentrations (ppm)

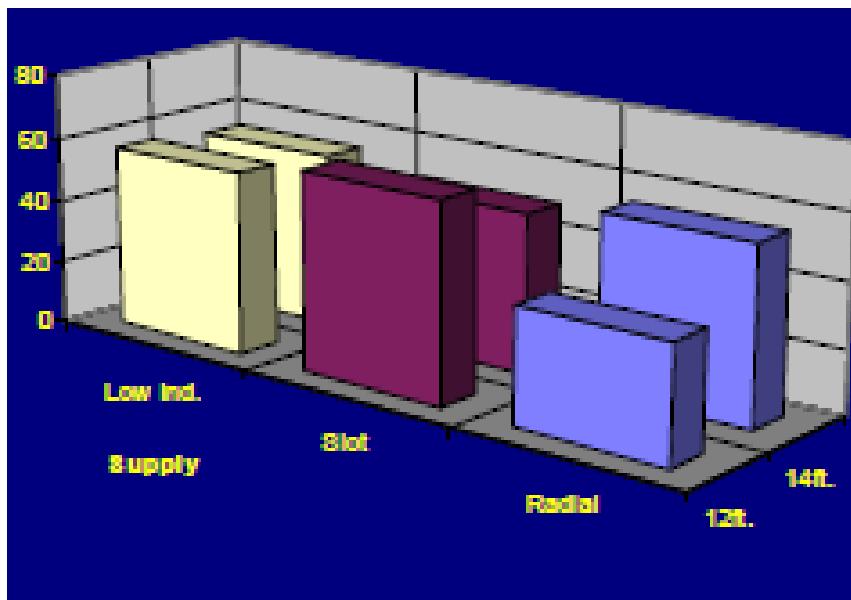


Figure 3.53 Comparison of Mean Breathing Zone CO₂ Concentrations (ppm)

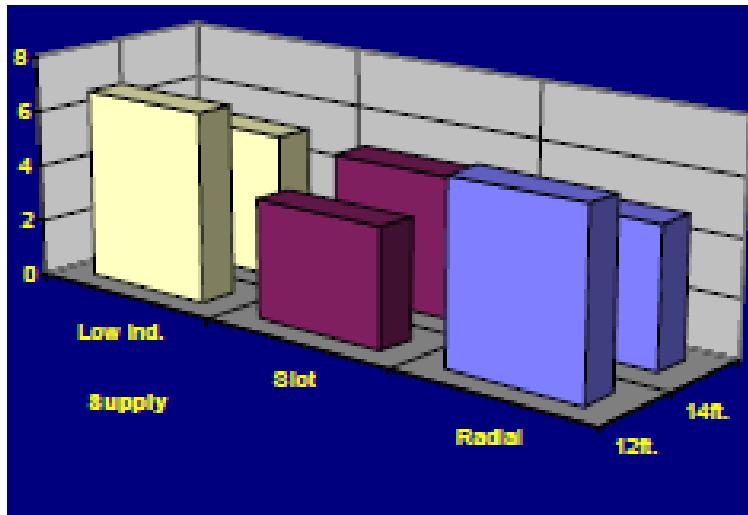


Figure 3.54 Comparison of Mean Cage NH_3 Concentrations (ppm)

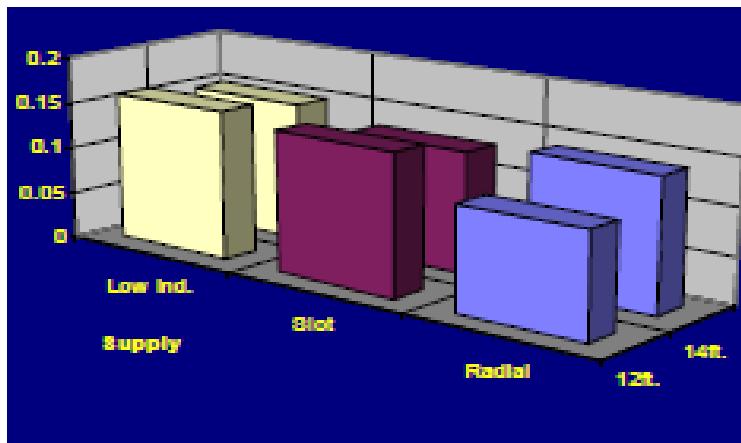


Figure 3.55 Comparison of Mean Breathing Zone NH_3 Concentrations (ppm)

The in-cage values are slightly reduced for both the radial and low-induction supply diffusers, while the room values show little change or some increase. As is often the case, improving the cage ventilation seems to degrade the room performance.

3.1.9 Supply Temperature

The experimental data for the generation of NH_3 indicate that NH_3 is produced at a higher rate when the relative humidity is high. As the relative humidity decreases with increasing

temperature it was expected that the NH₃ concentrations in the cages and room would be related to the supply temperature.

Figures 3.56 and 3.57 show the cage and room temperatures plotted against the supply temperature. As expected, the higher the supply temperature the higher the cage and room temperatures, although there is a wide variation as was noted previously. The choice of exhaust location has a strong influence on the room and cage temperature.

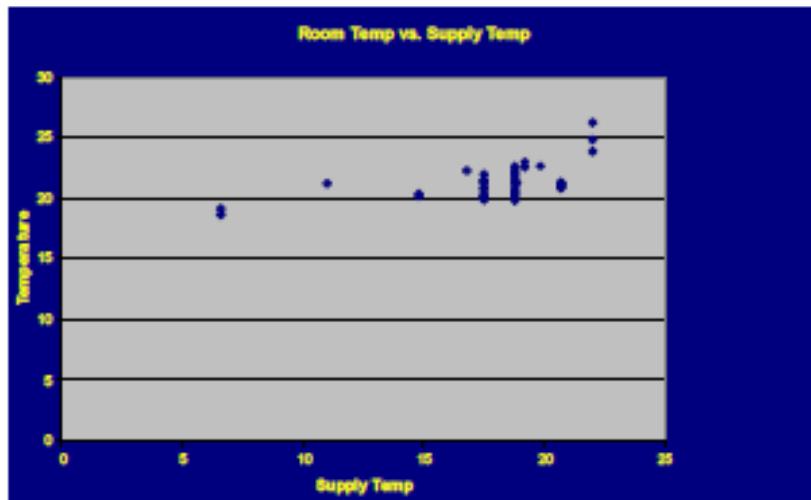


Figure 3.56 Room Breathing Zone Temperature vs. Supply Discharge Temperature

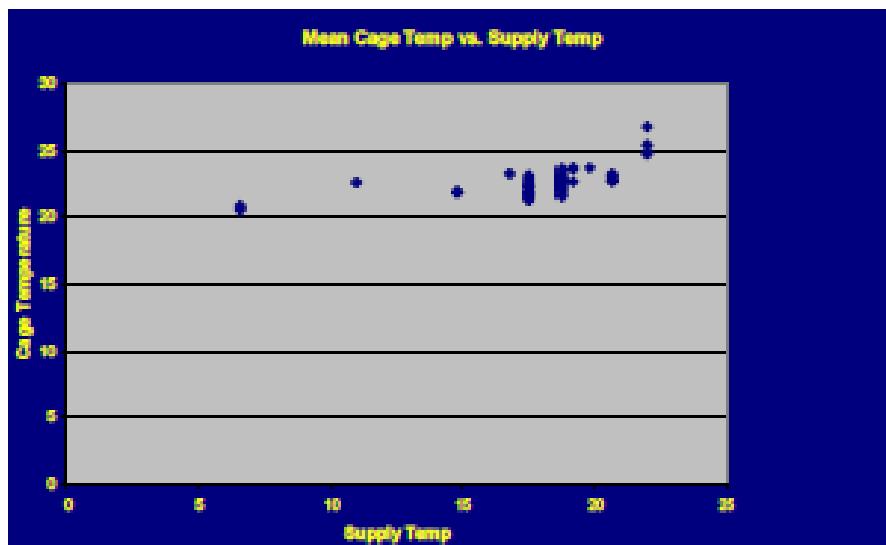


Figure 3.57 Mean Cage Temperatures vs. Supply Discharge Temperature

Figures 3.58 and 3.59 show the cage and room NH₃ concentrations on day 4 plotted against supply relative humidity (RH). The cage values show no notable trend with quite a wide variation at the standard supply RH of 61 percent. However, even though there is some scatter in the data, the room NH₃ concentration plot shows a clear trend to higher values at higher supply RH.

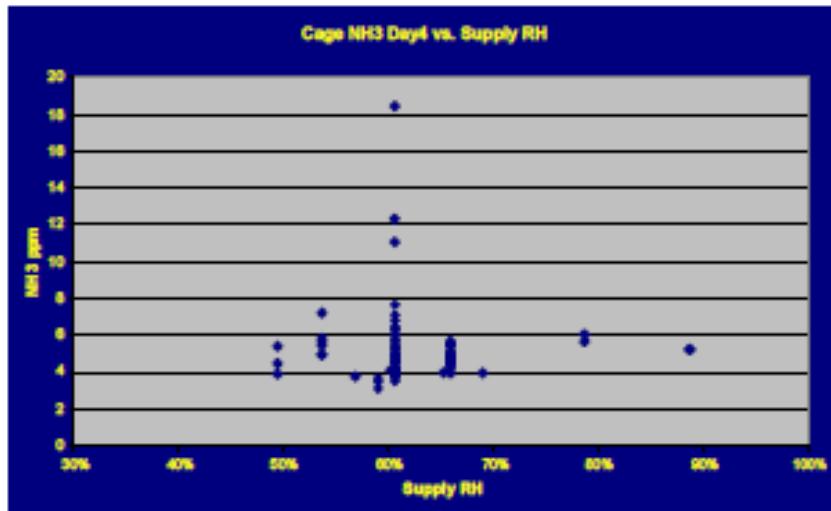


Figure 3.58 Cage NH₃ Concentration vs. Supply Relative Humidity

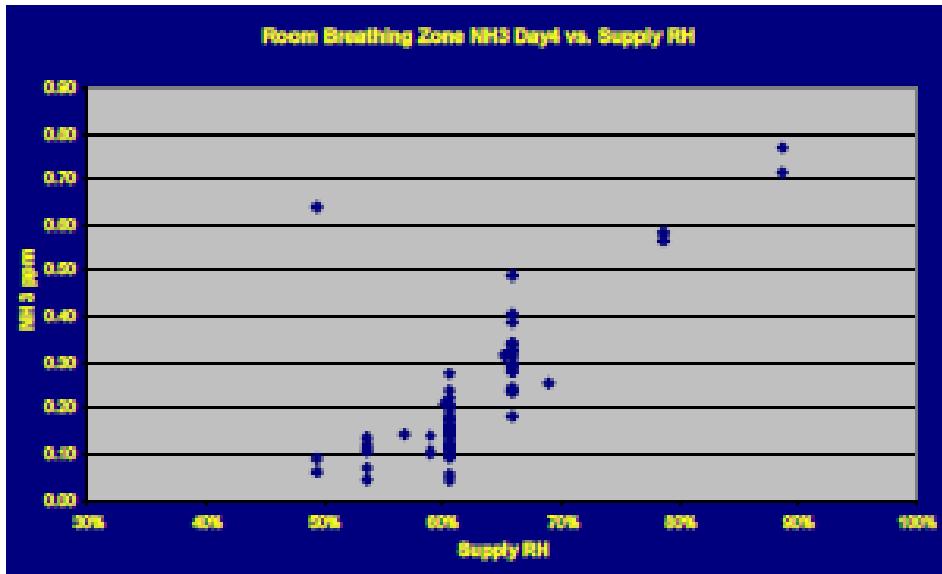


Figure 3.59 Room Breathing Zone NH_3 Concentration vs. Supply Relative Humidity

Cases 99 to 101 were run with a supply temperature of 22.2°C (72.0°F). Case 99 was the same as the basecase (radial supply ceiling exhaust), case 100 was the same as case 3 (radial supply low level exhaust) and case 101 was the same as case 66 (low induction supply, low level exhaust, 5 ACH). These cases were run to investigate the effect of increased temperatures in the room, in particular the reduction of relative humidity and NH_3 generation that should result.

Raising the supply temperature for these cases produces an increase in both room and cage temperature as shown in table 3.02

Table 3.02 Comparison of Temperatures $^\circ\text{C}$ ($^\circ\text{F}$)

	Case 01	Case 99	Case 03	Case 100	Case 66	Case 101
Room BZ	20.3 (68.5)	23.9 (75.0)	22.7 (72.9)	24.8 (76.6)	18.6 (65.5)	26.2 (79.2)
Cage Mean	22.1 (71.8)	24.8 (76.6)	23.4 (74.1)	25.4 (77.7)	20.6 (69.1)	26.8 (80.2)
Cage Max	23.0 (73.4)	25.7 (78.3)	24.6 (76.3)	26.8 (80.2)	21.9 (71.4)	28.3 (82.9)

Cases 99 and 100 represent an increase of 3.2°C (5.8°F) in the supply temperature and produce an increase of around 2.5°C (4.5°F) in both room and cage temperature. Case 101 represents an increase of 15.4°C (27.7°F) in the supply temperature. This raises the room and cage temperature by nearly 8.0°C (14.4°F). The maximum temperature in a cage is increased to around 28.0°C (82.4°F). Although it is high, is still likely to be more than acceptable to the mice.

Case 99 produces an improvement in NH_3 concentration in the room of nearly 50 percent and nearly 30 percent in the cage.

Cases 100 and 101 do not produce the same level of improvement as the original cases 3 and 66, which already have very low humidity values (below the 61 percent minimum from the experimental data), and so the reduction in humidity does not produce a lower NH₃ generation rate.

To further investigate the effect of increasing supply temperature (without re-running all 101 cases) the data was “post-processed” by adding 3.2 °C (5.8 °F) to the mean temperature for each cage. This is equivalent to raising the supply temperature by approximately 4.0 °C (7.2 °F).

Figures 3.60 and 3.61 show the resulting bar charts for the day 4 cage and room NH₃ concentrations together with the original data. These charts clearly show the reduction in NH₃ concentrations that can be expected when an increased supply temperature is used. A few of the cases do not show significant improvements. These are cases where the original run is already at the minimum RH (61 percent) used in the generation rate calculation.

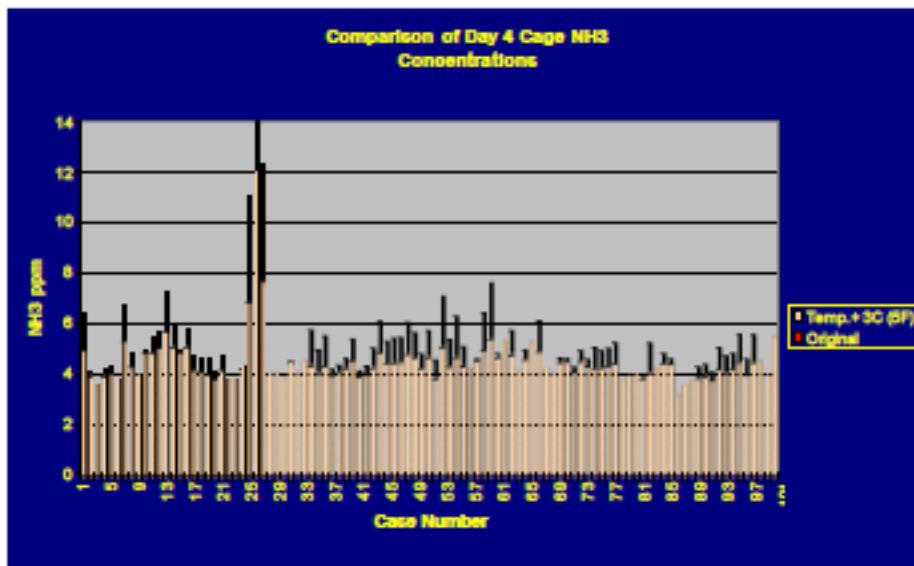


Figure 3.60 Comparison of Cage Day 4 NH₃ Concentrations

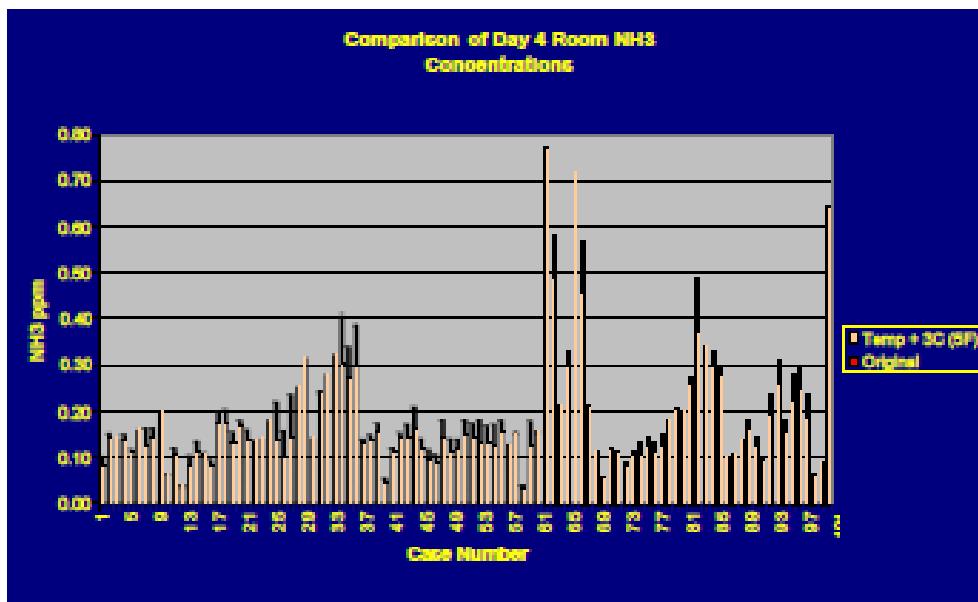


Figure 3.61 Comparison of Room Day 4 NH₃ Concentrations

3.2 NH₃ Concentrations for 10-day cycle

Table 3.03 shows a summary of mean and maximum NH₃ concentrations in the room's breathing zone over 10 days using the different generation rates measured in the experiments. In the summary, values between 0.5ppm and 1ppm have been colored blue, and values above 1 ppm are colored red. Smyth (1956) found 1ppm detected and identified by 10 subjects. In addition, analysis of data obtained in plant surveys conducted from 1965 to 1970 by the Bureau of Industrial Hygiene, Detroit Department of Health, found the limit of detection to be below 5 ppm and the complaint level to be 20 ppm to 25 ppm. Therefore, 1ppm was chosen as a conservative level at which people might be able to detect a smell in the room.

With the exception of the very low flow rates (5 ACH) for the double density rooms, all the room configurations show an acceptable NH₃ concentration, on average, in the breathing zone up to day 5. The maximum value in the breathing zone, present in just one small location, is generally all right up to day 5. By day 5 and day 6 virtually all rooms had at least one spot above 1ppm. This indicates that changing the bedding every 5 days should leave most rooms with an acceptable atmosphere.

Table 3.04 shows a summary of mean and maximum NH₃ concentrations in the cages over 10 days using the different generation rates measured in the experiments. In the summary, values over 25 ppm have been colored red, as such high levels are likely to cause problems for the mice.

See Schoeb, Davidson and Lindsey (1982) who indicated that NH₃ concentrations above 25 ppm promote the growth of infective agents in the respiratory tract of rats in cages.

In cases 25-27, in which sealed edge cages with particularly poor ventilation are used (the only airflow is through the filter), the mean concentration did not rise above 25 ppm until day 7 for any of the rooms studied. The “maximum” part of the table shows that the worst cage in the room did go over 25 ppm on day 6 (see cases 73, 75, 77 and 78). By day 7 most rooms have at least one cage with NH₃ concentrations over 25 ppm.

As indicated previously, a supply rate of 0.85 cfm (4.01e-4 m³/s) per 100g mouse body weight will provide good room conditions up to day 4 or day 5. To go beyond this time before changing the bedding the flow rate must be increased to 1.28 cfm (6.04e-4 m³/s) per 100g, although a few rooms will be 1 ppm, on average, by day 7. Even increasing to 1.70 cfm (8.02e-4 m³/s) per 100g will only extend this to eight days, although even then the maximum NH₃ concentration in the breathing zone will rise to 3 ppm and some parts of the room will be noticeably smelly.

Even at 1.70 cfm (8.02e-4 m³/s) per 100g (20 ACH in the double density rooms) the cages are unacceptable by day 8 as the NH₃ concentration is around 25ppm. The very small amount of improvement that 20 ACH gives over 15 ACH for the cages makes it unlikely that further increases in supply flow rates will change this situation.

Tables 3.05 and 3.06 are repeats of 3.03 and 3.04 with the cage temperatures increased by 3.0 °C (5.4 °F). The increase in temperature reduces the relative humidity as well as the NH₃ generation rate leading to lower NH₃ concentrations.

Increasing the temperature is also recommended by Gordon, Becker and Ali (1997) who indicate that the “standard housing temperature of 22.0-24.0 °C (72.0-75.0 °F) is significantly below the thermoneutral zone of groups of mice suggesting that they are subjected to varying degrees of cold stress under standard housing conditions.”

The increase in temperature shows the rooms improve in approximately one day. Considering the average NH₃ concentration, the rooms are acceptable up to day 7 apart from the very low flow rates that fail on day 6. The maximum NH₃ concentration shows an improvement with many more rooms acceptable on day 5 with most starting to fail on day 6.

The cages show nearly a two day improvement with the average cage going over 25 ppm on day 10, although the worst cages with the maximum NH₃ concentration start to fail in a few rooms on day 8, with most failing on day 9.

Note on use of tables 3.03 to 3.06:

The tables show mean NH₃ concentrations for the cages and scientist's breathing zone (1.5m-1.8m, 4'11" – 5' 11") and the maximum value (in one cage or one spot in the room breathing zone). The color coding allows both good (black) and poor (red) cases to be quickly identified. It

is also possible to see how quickly the NH₃ concentrations deteriorate over the 10-day cycle for the particular case.

3.3

Ranking of Whole Room Simulations

The following tables (3.07 to 3.14) present rankings of the results of the CFD room simulations based on room (scientist's breathing zone) and cage mean values for temperature, relative humidity, and CO₂ and NH₃ (day 4) concentrations. The tables start with the case with the lowest value and list the rest in ascending order. In addition to the case number, which should be used to identify all details of the case, the supply diffuser type, exhaust location, supply flow rate, and supply discharge temperature are given to provide a quick overview of the case.

Tables 3.07 and 3.08 for temperature show the ceiling exhausts produce lower temperatures in both the room and cages, ignoring the two 5 ACH cases which start with very low supply temperatures. Tables 3.09 and 3.10 for relative humidity show that the low exhaust cases seem to dominate the table producing low humidity. This is also a consequence of the low exhaust rooms and cages being warmer than the ceiling and high level exhausts.

Table 3.11 showing room breathing zone CO₂ concentration shows the ceiling and high level exhausts producing the lowest values. The overall variation is very small in absolute terms. It is interesting to see that the first 20 ACH case comes 50th in the list. This indicates that with the right design it is possible to ventilate a room better than by simply providing more air.

Table 3.12 showing CO₂ concentration in the cages also shows relatively small variations across the cases. No particular configuration presents itself as always performing better than the others.

Tables 3.13 and 3.14 show NH₃ concentrations in the room and cages on day 4. The room data shows no particular pattern. The cage data shows rather more low exhaust cases giving low values, which is due to the higher temperature and related lower relative humidity reducing the actual NH₃ generation rate.

In all of the ranking tables, no single configuration proves to be superior in all respects. This further illustrates that the airflow patterns and thus the ventilation of the room and the cages depends on the complex interaction of all of features in the room.

Table 3.14 Ranking of Cases with respect to Cage NH₃ (Day 4)

Case Name	Supply Diffuser Type	Exhaust Location and Number	Supply ACH	Supply Temperature (°C)	Supply Temperature (°F)	Cage NH ₃ (day 4) (ppm)
Case 87	Radial	Low	15	19.2	66.6	3.13
Case 88	Slot	Low	15	19.2	66.6	3.49
Case 03	Radial	Low	15	18.8	65.8	3.53
Case 89	Low Ind	Low	15	19.2	66.6	3.68
Case 79	Radial	2 Door exhausts	15	18.8	65.8	3.70
Case 23	Slot	Low	15	18.8	65.8	3.71
Case 06	Slot	Low	15	18.8	65.8	3.72
Case 30	Low Ind	Low	20	19.8	67.6	3.75
Case 22	Radial	Low	15	18.8	65.8	3.77
Case 80	Slot	2 Door exhausts	15	18.8	65.8	3.84
Case 09	Low Ind	Low	15	18.8	65.8	3.88
Case 81	Low Ind	2 Door exhausts	15	18.8	65.8	3.92
Case 82	Radial	2 Door exhausts	15	18.8	65.8	3.92
Case 32	Slot	Low	15	17.5	63.5	3.93
Case 28	Low Ind	Low	10	16.8	62.2	3.93
Case 69	Radial	High x4 / Low x4	15	18.8	65.8	3.94
Case 29	Low Ind	Low	5	11	51.8	3.97
Case 92	Low Ind	Ceiling	15	18.8	65.8	4.02
Case 02	Radial	High	15	18.8	65.8	4.03
Case 20	Slot	Ceiling	15	18.8	65.8	4.04
Case 41	Slot	Ceiling x4	15	18.8	65.8	4.06
Case 64	Low Ind	Low	20	18.9	66.0	4.07
Case 37	Radial	Ceiling/Low 50/50	15	18.8	65.8	4.13
Case 68	Low Ind	Low	20	18.9	66.0	4.13
Case 84	Low Ind	2 Door exhausts	15	17.5	63.5	4.17
Case 57	Radial	Low	15	18.8	65.8	4.17
Case 04	Slot	Ceiling	15	18.8	65.8	4.18
Case 72	Radial	High x4 / Low x2	15	18.8	65.8	4.22
Case 90	Radial	Ceiling	15	18.8	65.8	4.22
Case 05	Slot	High	15	18.8	65.8	4.23
Case 24	Low Ind	Low	15	18.8	65.8	4.24
Case 42	Low Ind	Ceiling x4	15	18.8	65.8	4.25
Case 38	Slot	Ceiling/Low 50/50	15	18.8	65.8	4.28
Case 91	Slot	Ceiling	15	18.8	65.8	4.33
Case 33	Low Ind	Low	15	17.5	63.5	4.44
Case 31	Radial	Low	15	17.5	63.5	4.45
Case 52	Radial	Ceiling	15	18.8	65.8	4.49
Case 74	Low Ind	High x4 / Low x2	15	18.8	65.8	4.53
Case 97	Slot	Ceiling	15	17.5	63.5	4.54
Case 86	Slot	Low	15	17.5	63.5	4.54
Case 71	Low Ind	High x4 / Low x4	15	18.8	65.8	4.56
Case 58	Slot	High	15	18.8	65.8	4.58
Case 39	Low Ind	Ceiling/Low 50/50	15	18.8	65.8	4.58
Case 70	Slot	High x4 / Low x4	15	18.8	65.8	4.58
Case 19	Radial	Ceiling	15	18.8	65.8	4.61
Case 18	Low Ind	Ceiling	15	18.8	65.8	4.62
Case 94	Slot	Ceiling	15	17.5	63.5	4.66
Case 17	Slot	Ceiling	15	18.8	65.8	4.71
Case 61	Low Ind	Low	15	18.8	65.8	4.73
Case 21	Low Ind	Ceiling	15	18.8	65.8	4.73
Case 50	Radial	Ceiling	15	18.8	65.8	4.73

Case Name	Supply Diffuser Type	Exhaust Location and Number	Supply ACH	Supply Temperature (°C)	Supply Temperature (°F)	Cage NH ₃ (day 4) (ppm)
Case 85	Radial	Low	15	17.5	63.5	4.76
Case 95	Low Ind	Ceiling	15	17.5	63.5	4.77
Case 08	Low Ind	High	15	18.8	65.8	4.83
Case 76	Radial	Ceiling	15	18.8	65.8	4.85
Case 73	Slot	High x4 / Low x2	15	18.8	65.8	4.87
Case 65	Low Ind	Low	15	17.5	63.5	4.90
Case 35	Slot	Ceiling	15	17.5	63.5	4.90
Case 77	Slot	Ceiling	15	18.8	65.8	4.94
Case 10	Radial	Ceiling	15	20.7	69.3	4.94
Case 15	Low Ind	Low	15	20.7	69.3	4.94
Case 43	Low Ind (rot 90°)	Ceiling	15	18.8	65.8	4.96
Case 93	Radial	Ceiling	15	17.5	63.5	4.97
Case 75	Radial	Ceiling/Low 50/50	15	18.8	65.8	4.98
Case 56	Radial	High	15	18.8	65.8	5.01
Case 83	Slot	2 Door exhausts	15	17.5	63.5	5.15
Case 78	Low Ind	Ceiling	15	18.8	65.8	5.16
Case 66	Low Ind	Low	5	6.6	43.9	5.21
Case 45	Radial	Ceiling	15	18.8	65.8	5.22
Case 62	Low Ind	Low	5	6.6	43.9	5.23
Case 54	Slot	Ceiling	15	18.8	65.8	5.32
Case 40	Radial	Ceiling x4	15	18.8	65.8	5.33
Case 46	Radial	Ceiling	15	18.8	65.8	5.35
Case 47	Radial	Ceiling	15	18.8	65.8	5.36
Case 11	Radial	Low	15	20.7	69.3	5.42
Case 36	Low Ind	Ceiling	15	17.5	63.5	5.44
Case 98	Low ind	Ceiling	15	17.5	63.5	5.50
Case 96	Radial	Ceiling	15	17.5	63.5	5.51
Case 49	Radial	Ceiling	15	18.8	65.8	5.56
Case 51	Radial	Ceiling	15	18.8	65.8	5.64
Case 63	Low Ind	Low	10	14.8	58.6	5.64
Case 12	Slot	Ceiling	15	20.7	69.3	5.66
Case 34	Radial	Ceiling	15	17.5	63.5	5.66
Case 16	Radial	Ceiling	15	18.8	65.8	5.76
Case 14	Low Ind	Ceiling	15	20.7	69.3	5.82
Case 48	Radial	Ceiling	15	18.8	65.8	5.98
Case 44	Radial (rot 90°)	Ceiling	15	18.8	65.8	6.03
Case 67	Low Ind	Low	10	14.8	58.6	6.03
Case 55	Low Ind	Ceiling	15	18.8	65.8	6.22
Basecase	Radial	Ceiling	15	18.8	65.8	6.33
Case 59	Slot	Low	15	18.8	65.8	6.38
Case 07	Low Ind	Ceiling	15	18.8	65.8	6.71
Case 53	Radial	Ceiling	15	18.8	65.8	7.02
Case 13	Slot	Low	15	20.7	69.3	7.21
Case 60	Low Ind	High	15	18.8	65.8	7.56
Case 25	Radial	Ceiling	15	18.8	65.8	11.05
Case 27	Low Ind	Ceiling	15	18.8	65.8	12.31
Case 26	Slot	Ceiling	15	18.8	65.8	18.42

3.4 Recommendations

There were a total of 101 typical animal room and ventilation configurations analyzed by CFD simulation and subjected to rigorous quantitative post-processing. The analysis focused on CO₂ and NH₃ concentrations in the scientist's breathing zone (4'11" - 5'11", 1.5m to 1.8m) and in the cages occupied by mice. As stated in section 3.2, the nominal pass/fail limits chosen were 1 ppm NH₃ in the breathing zone and 25 ppm NH₃ in the cage.

The results of the CFD simulations performed in this study show that no particular room layout or ventilation system produces consistently good or bad results. Indeed, often improvements in the room are accompanied by poorer ventilation in the cages. The CO₂ concentration values are representative of any airborne contaminants, whereas the NH₃ concentrations that are related to the CO₂ concentrations also depend on temperature and relative humidity.

The level of CO₂ concentration in the room breathing zone depends on both the flow rate into the room and the number of cages, and mice present in the room. Doubling the number of cages leads to approximately double the amount of CO₂. Rooms with low stocking density could be operated with lower flow rates;

Acceptable day 5 NH₃ concentrations are produced by supply flow rates of 0.85cfm (4.01e-4 m³/s) per 100g body weight of mice (equivalent to 5 ACH for single density racks, 10 ACH for double density racks);

Acceptable day 6 NH₃ concentrations are produced by supply flow rates of around 1.28cfm (6.04e-4 m³/s) per 100g body weight of mice (equivalent to 7.5 ACH for single density racks, 15 ACH for double density racks);

Changing bedding every four to five days will produce acceptable rooms (at supply flow rates of around 0.85 cfm (4.01e-4 m³/s) per 100g body weight of mice) and acceptable cage environments for the mice;

Increasing the cage temperature by 3.0 °C (5.4 °F) could extend the period for changing to six or seven days, and can provide a better environment for the mice;

Ceiling level exhausts often provide poor ventilation for cages, compared with low level exhausts;

Although increasing the ventilation rate reduces the concentration of contaminants in the occupied zone of the room by increased dilution, the same cannot be said for cage concentrations. In fact, with single cage density, the cage concentrations of NH₃ were seen to rise with ventilation rates increasing from 15 to 20 ACH;

Higher temperatures in the room and cages reduce the relative humidity, and NH₃ generation and concentrations. Although this can be achieved by low level exhausts (which consistently

appear to produce higher temperatures) it is better achieved by increasing the supply discharge temperature for high level and ceiling exhausts, resulting in less cooling in the room and, therefore, lower running costs.

The experimental measurement of NH₃ generation shows dependency on relative humidity. As relative humidity is dependent on temperature (if the level of moisture in the air is constant), raising the temperature in the room and cages will reduce the levels of NH₃. Further, as indicated in the study by Gordon, Becker and Ali (1997), increasing the cage temperatures above the normal 22.0 to 23.0 °C (72.0 to 74.0 °F) is likely to provide a more comfortable environment for the mice. A recommendation of this study is that the supply discharge temperatures should be increased by 3.0 to 4.0 °C (5.4 to 7.2 °F) to about 23.0 °C (73.4 °F). This will provide room temperatures around 25 °C (77 °F) and cages with a temperature of about 26.0 °C (78.8 °F), though a few individual cages may rise as high as 28.0 °C (82.4 °F).